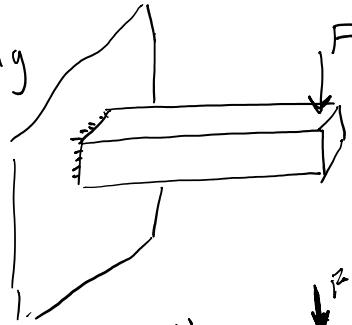


1-31-22

For the beam under bending

$$\tau_b = \frac{Mc}{I_t}$$



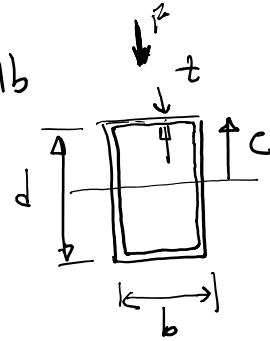
where

$$M = FL = 1000(12) = 12000 \text{ in-lb}$$

$$c = \frac{4}{2} = 2''$$

$$I_t = I_u \cdot t = 26.67(0.177)$$

$$I_t = 4.72 \text{ in}^4$$



where

 $I_u = \text{unit (or per inch)}$

$$I_u = \frac{d^2}{6} (3b + d) \quad [\text{Table 9-2}]$$

where

$$b = 2$$

$$d = 4$$

$$I_u = \frac{4^2}{6} (3 \cdot 2 + 4) = 26.67 \text{ in}^3$$

where

$$t = 0.707 h$$

$$= 0.707 (0.25) = 0.177''$$

Psi

$$\text{Therefore } \tau_b = \frac{Mc}{I_t} = \frac{12000(2)}{4.72} = 5085$$

Calculating shear stress due to direct

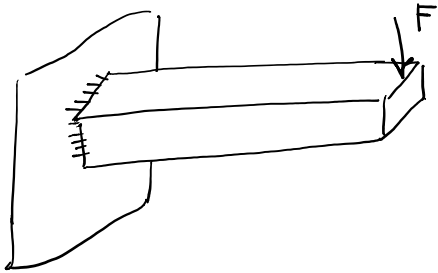
$$\text{Shear force } \tau_d = \frac{F}{A_t} = \frac{1000}{2.124} = 470.8 \text{ Psi}$$

where

$$A_t = (2+2+4+4)(0.177)$$

$$A_t = 2.124 \text{ in}^2$$

How Do we Combine the Two τ_b and τ_d ?



$\tau_b \equiv$ out of Plane of weld (OOP)

$\tau_d \equiv$ in plane of weld (IP)

Code says: Combine these stress vectorially

$$\tau = \sqrt{\tau_b^2 + \tau_d^2} = 5106.7 \text{ PSI}$$

Strength

$$S_{ys} = 0.3 S_{ut}$$

Code says use S_{ut} associated with the weakest of weld rod or base metal in its Hot-rolled condition

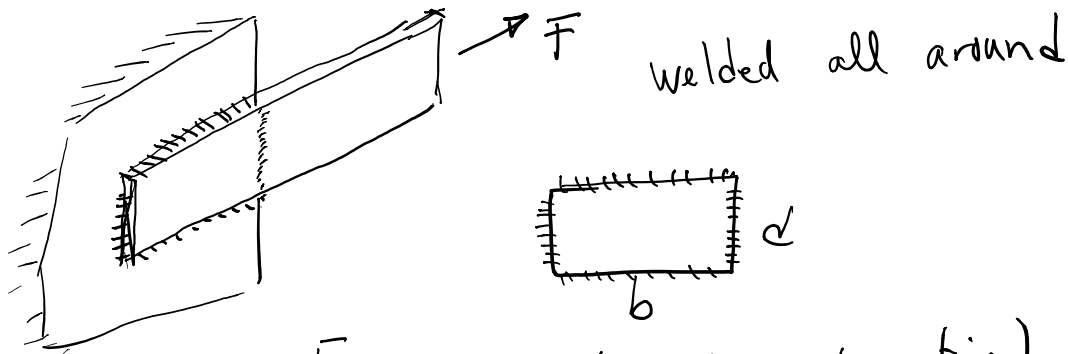
Assuming base metal is stronger than weld rod metal

$$S_{ys} = 0.3 (70) = 21 \text{ KSi}$$

$$n = \frac{S_{ys}}{\tau} = \frac{21000}{5106.7} = 4.1 \leftarrow$$

Acceptable

Direct shear loading (no bending / torsion / tension)



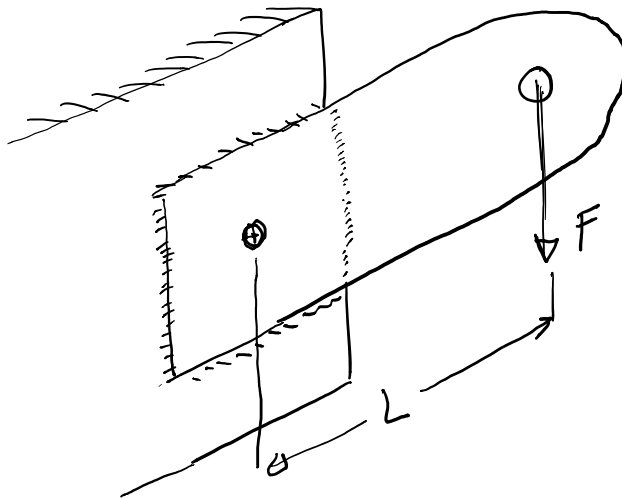
$$\tau = \frac{F}{A_t}$$

(In-Plane direction)

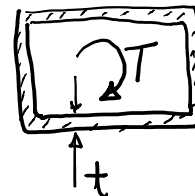
$$A_t = 2(b+d)t$$

$$\text{and } t = 0.707 h$$

Torsional loading

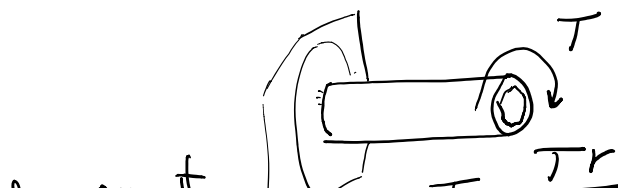


$$T = FL$$



$$\tau_t = \frac{Tr}{J_t}$$

where



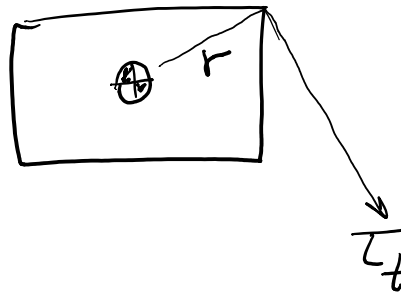
Where T = torsional moment (torque)



$$\tau_t = \frac{T r}{J}$$

= Force $\times$ distance from force to the Centroid of the weld pattern

r = the distance between the Centroid to any point that is being analysed ($r = r_{\max} = \max \tau$)

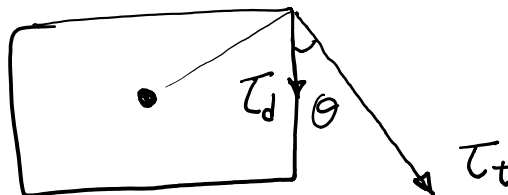


$\tau_t \equiv$ In-plane

$J_t \equiv$ Polar area moment of inertia of the weld with thickness of t

$$J_t = J_u t = J_u (0.707h)$$

$J_u =$ Unit polar area moment of inertia

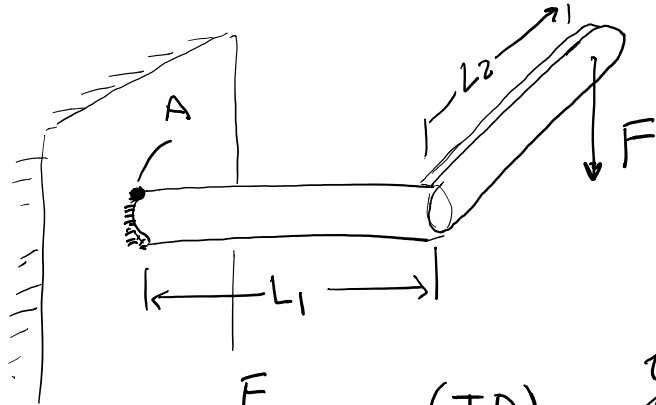


$$\tau_x = \tau_t \sin \theta$$

$$\tau_y = \tau_t \cos \theta + \tau_d$$

$$\tau = \sqrt{\tau_x^2 + \tau_y^2}$$

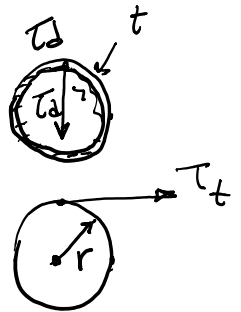
Combined Loading



Direct shear $\tau_d = \frac{F}{A_t}$ (IP)

Torsion $\tau_t = \frac{Tr}{J_t}$ (IP)

Bending $\tau_b = \frac{Mc}{I_t}$ (OOP)



$$T = FL_2$$

$$M = FL_1$$

Combine all IP stresses

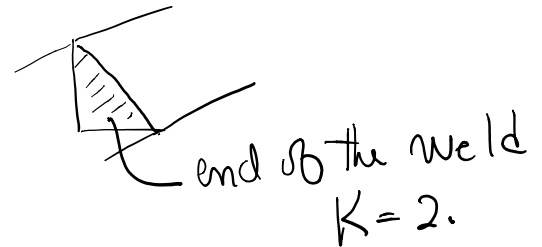
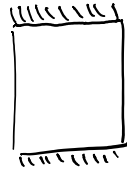
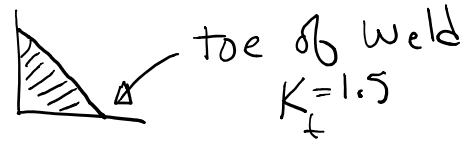
$$\tau_{IP} = \sqrt{\tau_d^2 + \tau_t^2}$$

$$\tau_{OP} = \tau_b$$

$$\Rightarrow \tau_{Res} = \sqrt{\tau_{IP}^2 + \tau_{OP}^2}$$

Compare to $0.3 S_u$

Do we take into account stress concentration factor?



Answer: Stress raisers are ignored for static loading but must be included for cyclic loading

Tables from the book

Table 9-1, 9-2 (I_u and J_u)

Table 9-3 Strength of the weld
(Last line fillet weld $S_{ys} = 0.3 S_u$)

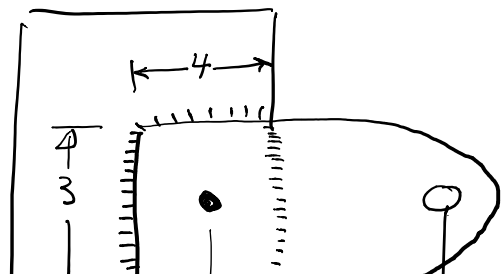
Table 9-5 Fatigue stress concentration factor

Example

E120 electrode

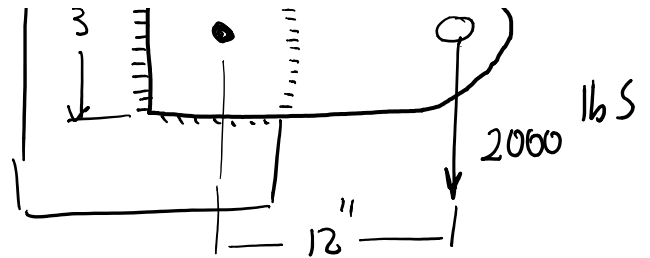
$h = 0.25"$

is $n > 3.5$?



11. <

is $n > 3.5$?



1) Find the throat

$$t = 0.707h = 0.177"$$

2) Find weld Area (throat)

$$A_t = t(3+3+4+4) = 2.475 \text{ in}^2$$

3) Calculate τ_d

$$\tau_d = \frac{F}{A_t} = \frac{2000}{2.475} = 808.2 \text{ PSI} \downarrow$$

4) Find the torsional moment

$$T = FL = 2000(12) = 24000 \text{ in-lb}$$

5) calculate τ_t

$$\tau_t = \frac{Tr}{J_t}$$

$$\text{where } T = 24000$$

$$r = \sqrt{2^2 + 1.5^2} = 2.5"$$

$$J_u = \frac{(d+b)^3}{6} = \frac{(3+4)^3}{6}$$

$$J_u = 57.17 \text{ in}^3$$

and

$$J_t = J_u \cdot t$$

in⁴

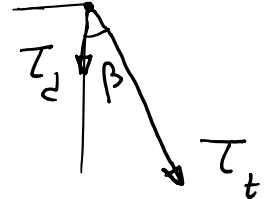
and

$$J_t = J_u \cdot \pi$$

$$= (57.17)(0.177) = 10.1 \text{ in}^4$$

$$\tau_t = \frac{T r}{J_t} = \frac{24000(2.5)}{10.1} = 5940.6 \text{ psi}$$

from geometry
 $\beta = 36.87^\circ$ degrees



6) Calculate resultant τ

$$\tau_{res}^2 = \tau_d^2 + \tau_t^2 + 2\tau_d\tau_t \cos \beta$$

OR $\tau_x = \tau_y = \tau = \sqrt{\tau_x^2 + \tau_y^2}$

$$\Rightarrow \tau = 6605 \text{ psi}$$

7) find weld strength in shear

$$S_{ys} = 0.35 \sigma_{ut}$$

$$S_{ys} = 0.3(120) = 36 \text{ Ksi}$$

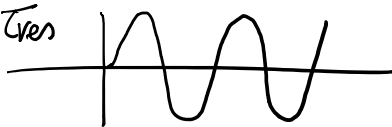
8) Factor of Safety

$$n = \frac{S_{ys}}{\tau_{res}} = \frac{36000}{6605} = 5.44$$

yes - acceptable

Weld Fatigue Analysis

- Find nominal stresses as before τ_{nom}
- Apply stress concentration factor τ_{act}

τ_{res}  Fully alternating stress

- Calculate S_{es} : endurance limit in shear

Calculating S_{es}

From fatigue analysis

$$S_e = K_a K_b \underbrace{K_c}_{(K_c)} K_d K_e K_f S'_e$$

Where $S'_e \equiv$ rotating bending endurance limit
(bending stress - Normal stress)

For steels

$$S'_e \cong 0.5 S_{ut} \quad (S_{ut} \leq 200 \text{ ksi})$$

Also $K_a \equiv$ Surface factor
