

ECE321 ELECTRONICS I

FALL 2006

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Lecture 7
17th October, 2006

CHAPTER 3

Diodes

3.7 Diode Physics

(3.8 Other Diode Types)

3.9 SPICE

Completely different
type of material
not circuits.

Also next lecture:
BJT device physics

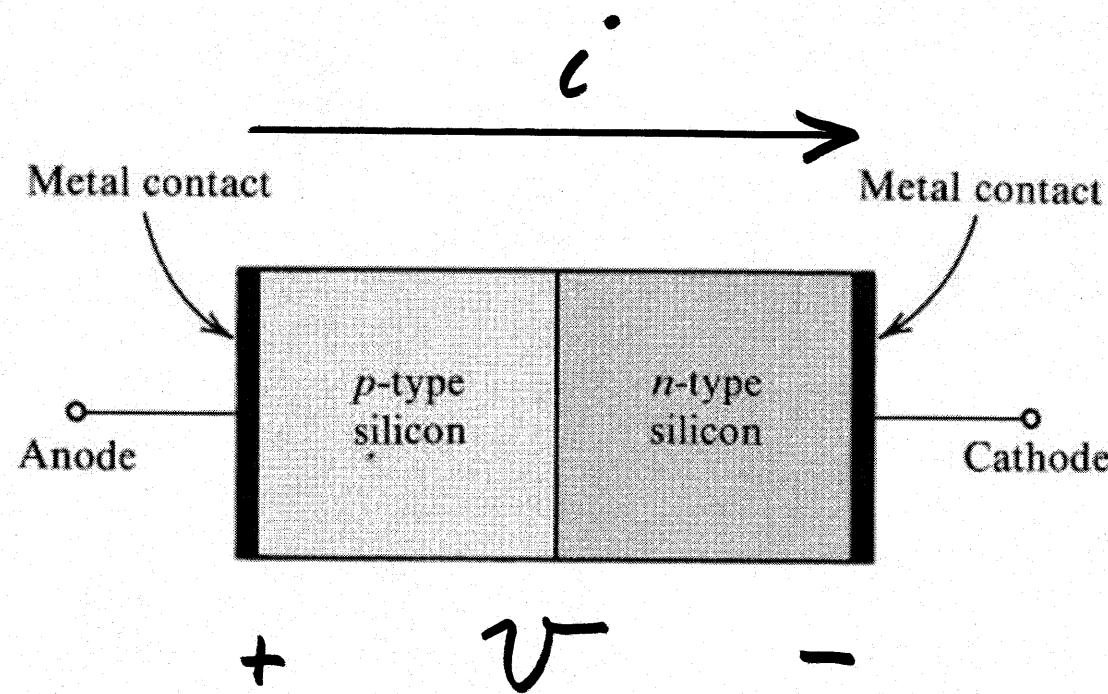
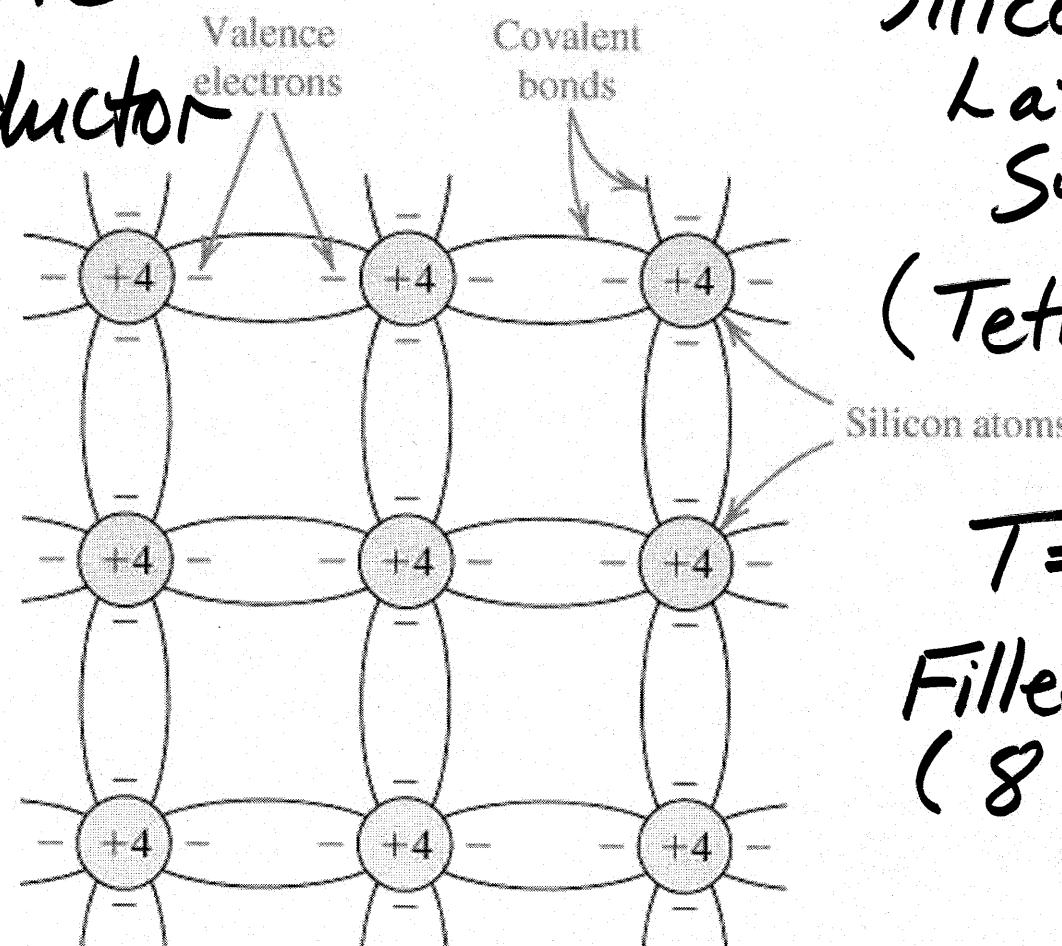


Figure 3.39 Simplified physical structure of the junction diode. (Actual geometries are given in Appendix A.)

Intrinsic Semiconductor



Silicon Lattice Structure (Tetrahedral)

$$T = 0^\circ K$$

Filled shells
(8 electrons)

Finite T →

Figure 3.40 Two-dimensional representation of the silicon crystal. The circles represent the inner core of silicon atoms, with +4 indicating its positive charge of $+4q$, which is neutralized by the charge of the four valence electrons. Observe how the covalent bonds are formed by sharing of the valence electrons. At 0 K, all bonds are intact and no free electrons are available for current conduction.

Finite $T \rightarrow$ lattice vibrations (phonons)

Electrons "free"

"Hole" motion
by adjacent
electron
hops.

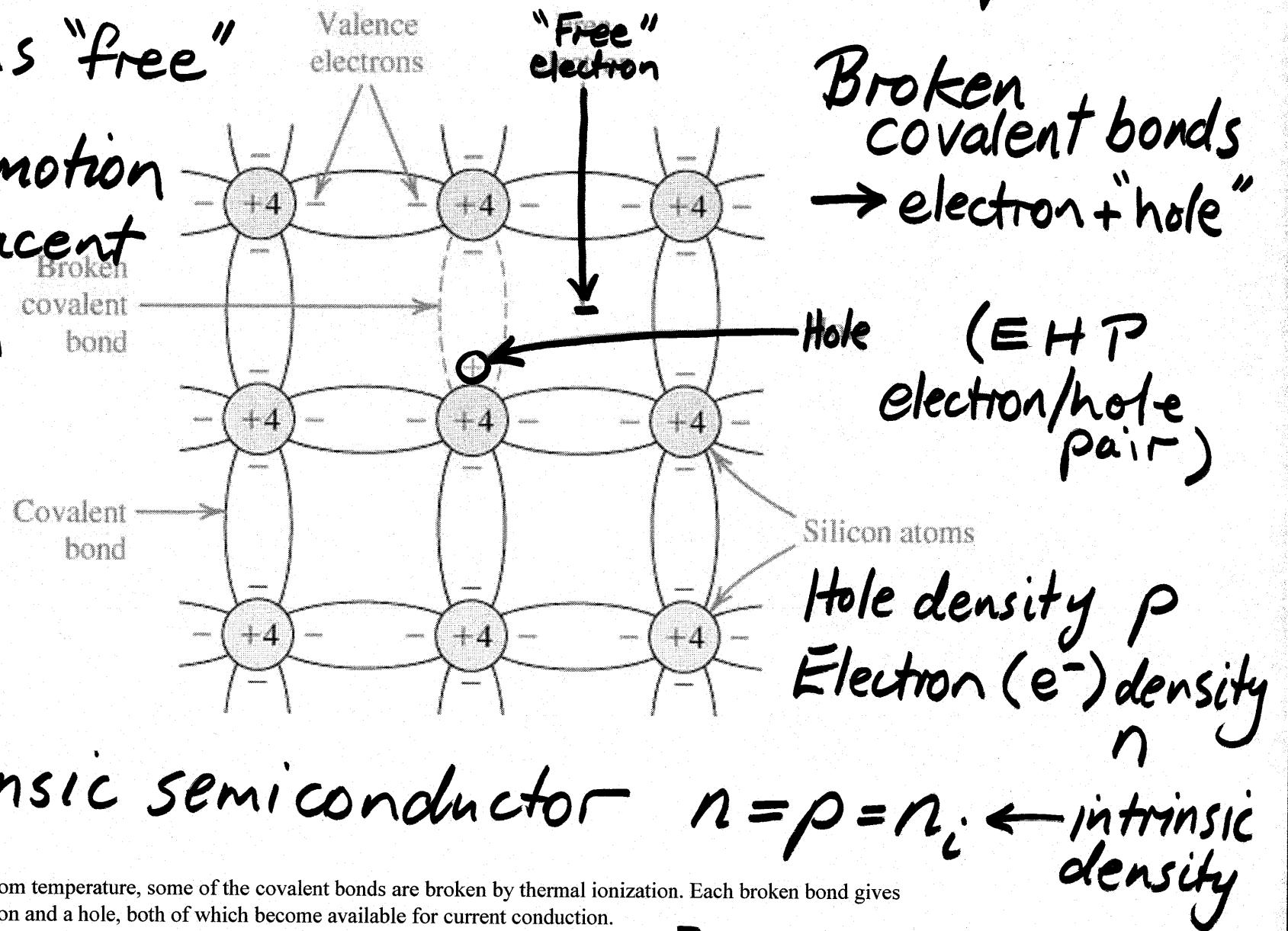


Figure 3.41 At room temperature, some of the covalent bonds are broken by thermal ionization. Each broken bond gives rise to a free electron and a hole, both of which become available for current conduction.

General rule : $np = n_i^2$

$$n_i^z = BT^3 \exp^{-E_g/kT}$$

↑ ↑ ↑
 n_i/cc $5.4 \times 10^{31} / (\text{K.cm}^2)^3$ Absolute T (K)

↑ ↑
 Boltzmann's constant
 $1.38 \times 10^{-23} \text{ J/K}$
 $= 8.62 \times 10^{-5} \text{ eV/K}$

For Si: $n_i = 1.5 \times 10^{10}/\text{cm}^3$

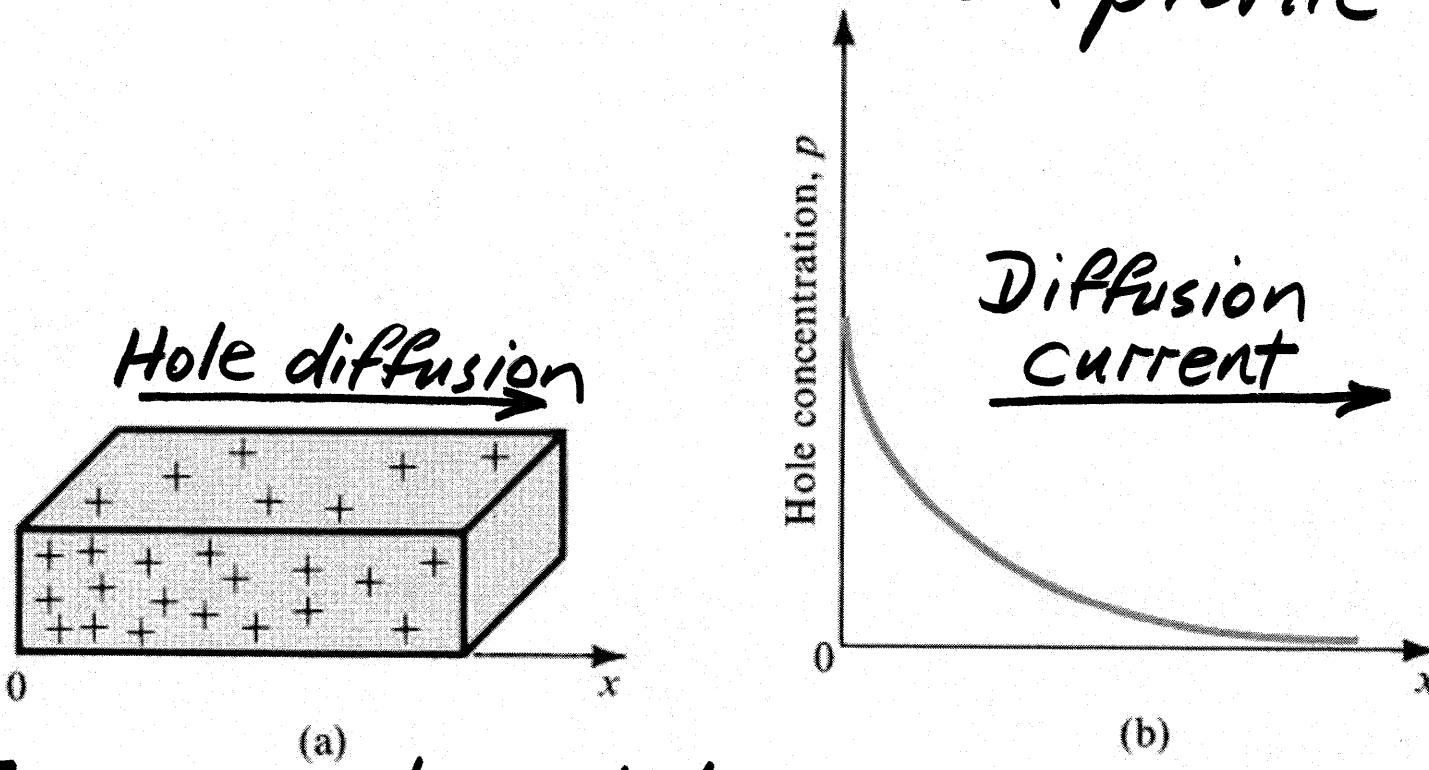
at $T = 300\text{K}$

(Compare 5×10^{22} atoms/ cm^3)

Energy "Band Gap"
 1.12eV for Si
 $(1.12 \times 1.6 \times 10^{-19} \text{ J})$

This is the energy required
 to break a covalent bond
 \rightarrow electron-hole pair
 (valence electron \rightarrow conduction e^-)

Diffusion : Density gradient Concentration profile



$$J_p = -q D_p \frac{dp}{dx} \quad \left(\frac{dp}{dx} < 0, \therefore J_p > 0 \right)$$

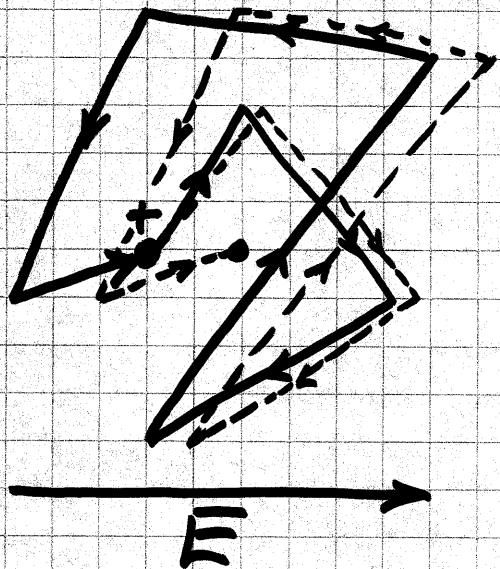
↑ Hole diffusion constant (diffusivity)

Figure 3.42 A bar of intrinsic silicon (a) in which the hole concentration profile shown in (b) has been created along the x-axis by some unspecified mechanism.

Holes: $J_p = -q D_p \frac{dp}{dx}$ $D_p \sim 12 \text{ cm}^2/\text{sec}$

Electrons: $J_n = q D_n \frac{dn}{dx}$ $D_n \sim 34 \text{ cm}^2/\text{sec}$

Drift Current (in an electric field)



Random thermal motion: no net effect

Superimpose small deviations due to electric field → small net motion

Small drift velocity << thermal velocities

$$\text{Holes: } v_{\text{drift}} = \mu_p E \quad \therefore J_p = q n \mu_p E$$

$$\text{Electrons: } v_{\text{drift}} = -\mu_n E \quad \therefore J_n = q n \mu_n E$$

Note: Electrons move opposite to E , but current direction opposite to v .

$$\therefore \text{Drift current } J_{\text{drift}} = q (n \mu_n + p \mu_p) E = \sigma E$$

$$\sigma = q (n \mu_n + p \mu_p) = 1/R$$

Intrinsic Si: $\mu_p \sim 480 \text{ cm}^2/\text{V.sec}$ $\mu_n \sim 1350 \text{ cm}^2/\text{V.sec}$

Note Einstein Relation: $J_n / \mu_n = J_p / \mu_p = kT / q = V_T$

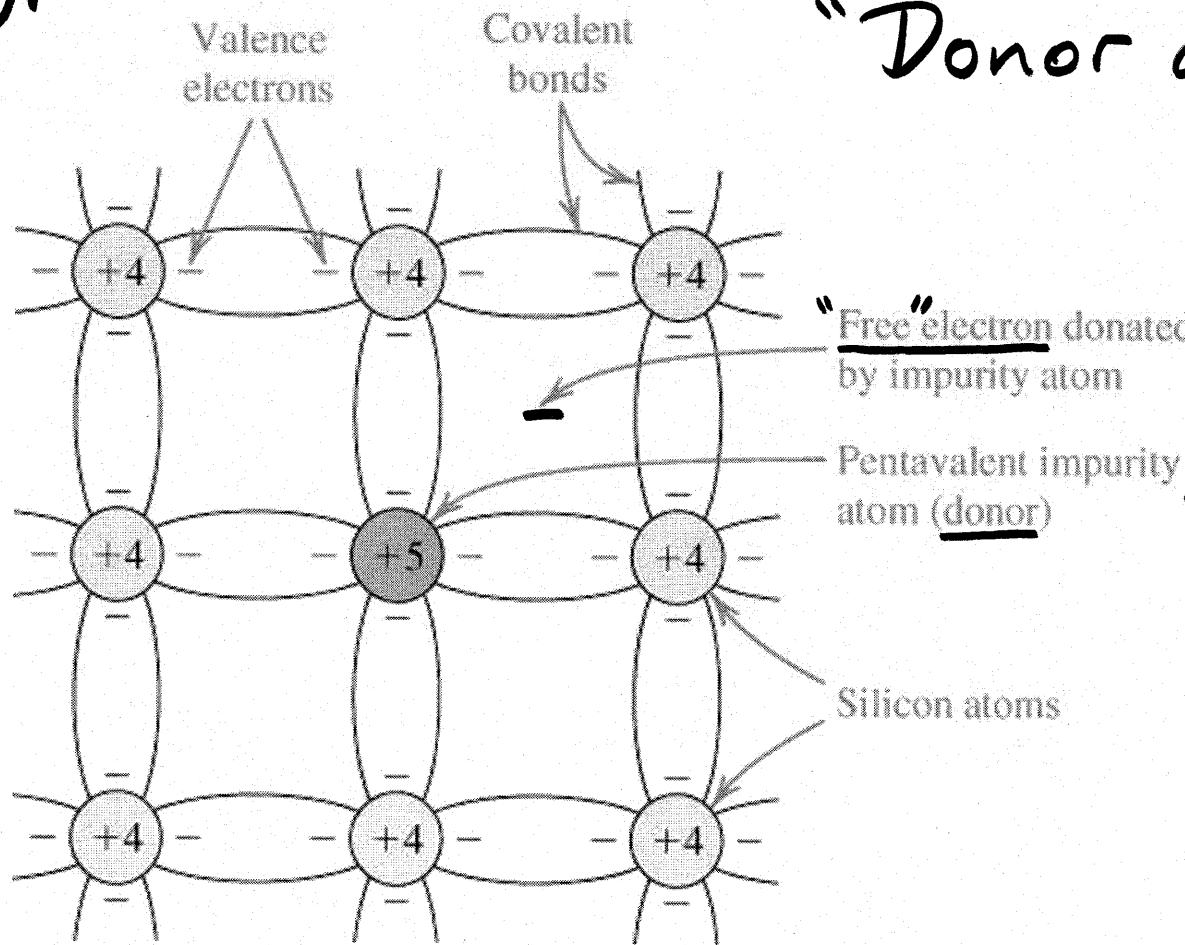
N-type Extrinsic Semiconductor

"Donor doping"

Majority carriers (electrons)

$$n_{NO} \approx N_D$$

\uparrow
thermal equilibrium



← e.g. P, As, Sb
doping

Minority carriers (holes) $np = n_i^2 \therefore \rho_{NO} \approx n_i^2 / N_D$

Figure 3.43 A silicon crystal doped by a pentavalent element. Each dopant atom donates a free electron and is thus called a donor. The doped semiconductor becomes n type.

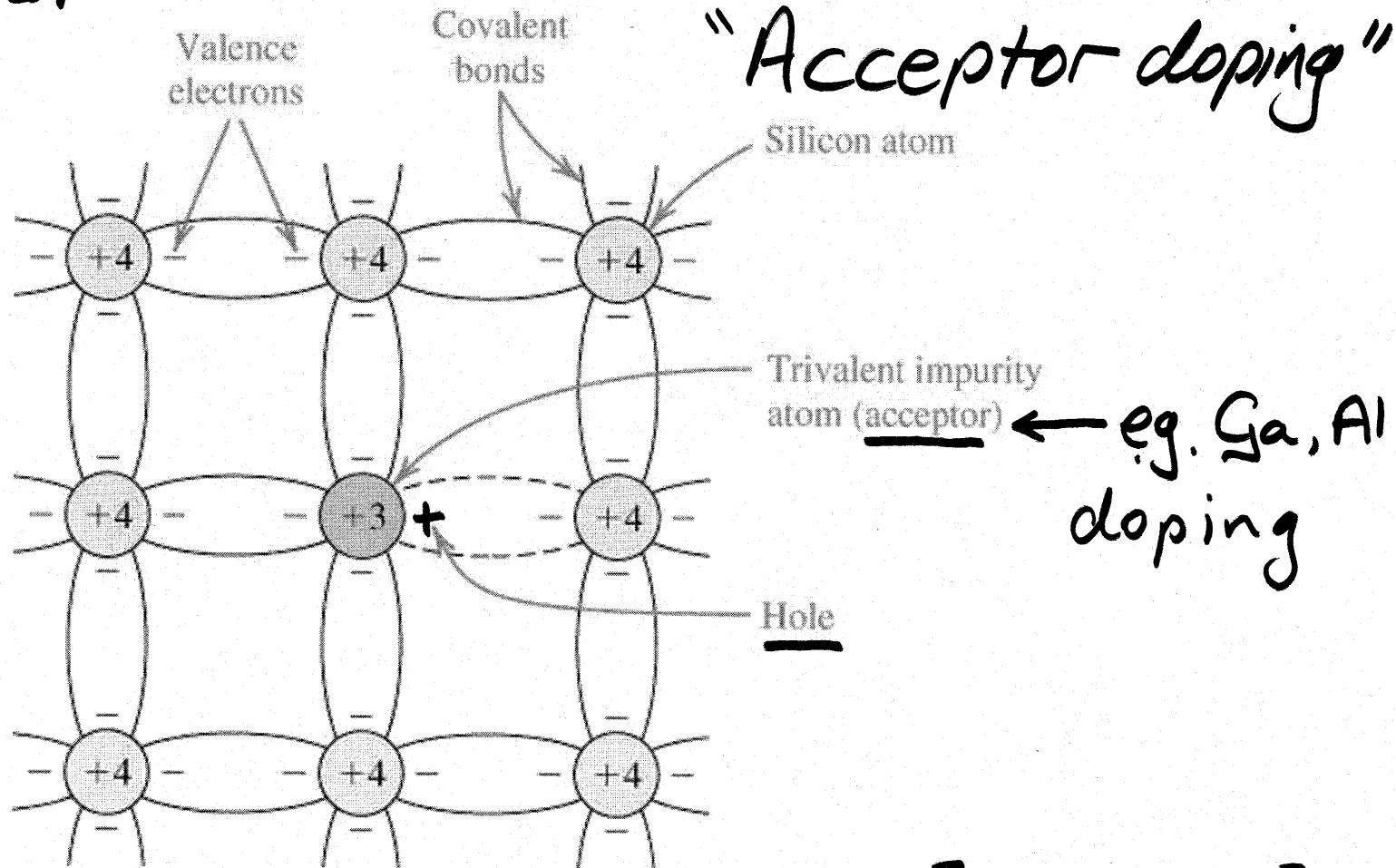
+ temperature dependent

Note : Electrically neutral (neg charges = pos charges)
 $(e^-s) n_{NO} = N_D (+ve ionized donors) + n_i^2 / N_D (+ve carriers)$

P-type Extrinsic Semiconductor "Acceptor doping"

Majority carriers (holes)

$$P_{p0} \approx N_A$$



Minority carriers (electrons) $n_p = n_i^2 \cdot \dots \cdot n_{p0} \approx n_i^2 / N_A$

Figure 3.44 A silicon crystal doped with a trivalent impurity. Each dopant atom gives rise to a hole, and the semiconductor becomes p type.

Electrically neutral: \rightarrow (positive charges = negative charges)
(Holes) $P_{p0} = N_A (-ve ionized acceptors) + n_i^2 / N_A$

Doping

Ex. 3.29

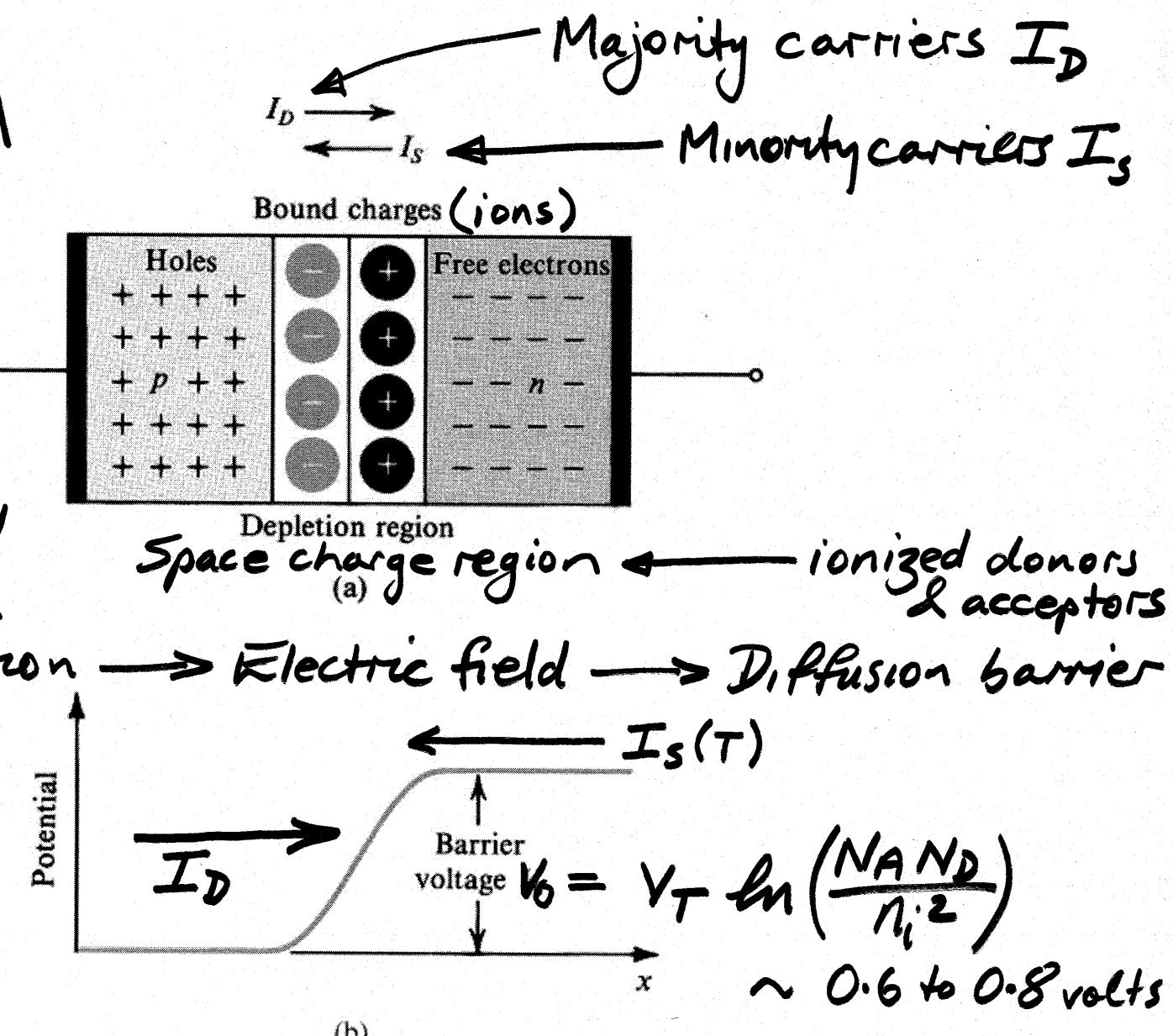
Ex. 3.30

Ex. 3.31

PN Junction

Holes & electrons
in space-charge
region recombine,
"uncovering" charged
donors/acceptors.

Charge separation \rightarrow Electric field \rightarrow Diffusion barrier



At equilibrium : $I_D = I_S$

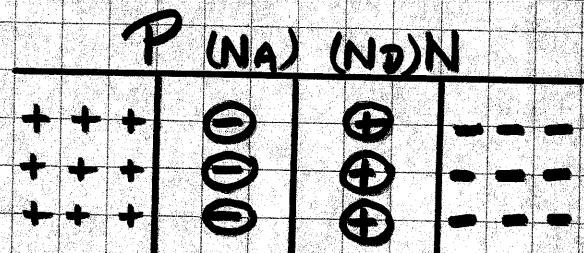
Figure 3.45 (a) The pn junction with no applied voltage (open-circuited terminals). (b) The potential distribution along an axis perpendicular to the junction.

I_D : Diffusion by majority carriers $\xrightleftharpoons[e^{-s}]{e^{-s}}$ impeded by field.

I_S : Minority carriers accelerated across region by field.

[Note: External voltage = 0]

Space Charge Region Width : (Depletion)



Negative charge = Positive charge

$$(q N_A) A x_p = (q N_D) A x_n$$

$$\therefore \frac{x_n}{x_p} = \frac{N_A}{N_D}$$

$$W_{\text{depl}} = x_n + x_p = \sqrt{\left(\frac{2\epsilon_{Si}}{q}\right) \left(\frac{1}{N_A} + \frac{1}{N_D}\right) V_0}$$

$\sim 0.1 \text{ to } 1 \mu\text{m}$

$$= x_n \left(1 + \frac{N_D}{N_A}\right) = x_p \left(1 + \frac{N_A}{N_D}\right)$$

$$\therefore x_n = \frac{N_A}{N_A + N_D} W_{\text{depl}} \quad \& \quad x_p = \frac{N_D}{N_A + N_D} W_{\text{depl}}$$

$$= \sqrt{\left(\frac{2\epsilon_{Si}}{q}\right) \frac{N_A / N_D}{N_A + N_D} V_0}$$

$$= \sqrt{\left(\frac{2\epsilon_{Si}}{q}\right) \frac{N_D / N_A}{N_A + N_D} V_0}$$

Note : $\epsilon_{Si} \approx 11.7 \epsilon_0 = 1.04 \times 10^{-12} \text{ F/cm}$

Ex. 3.32

Depletion region

Reverse Bias $I_D \xrightarrow{I_s}$ holes \rightarrow electrons
 $I_s \xleftarrow{\text{holes/electrons}}$

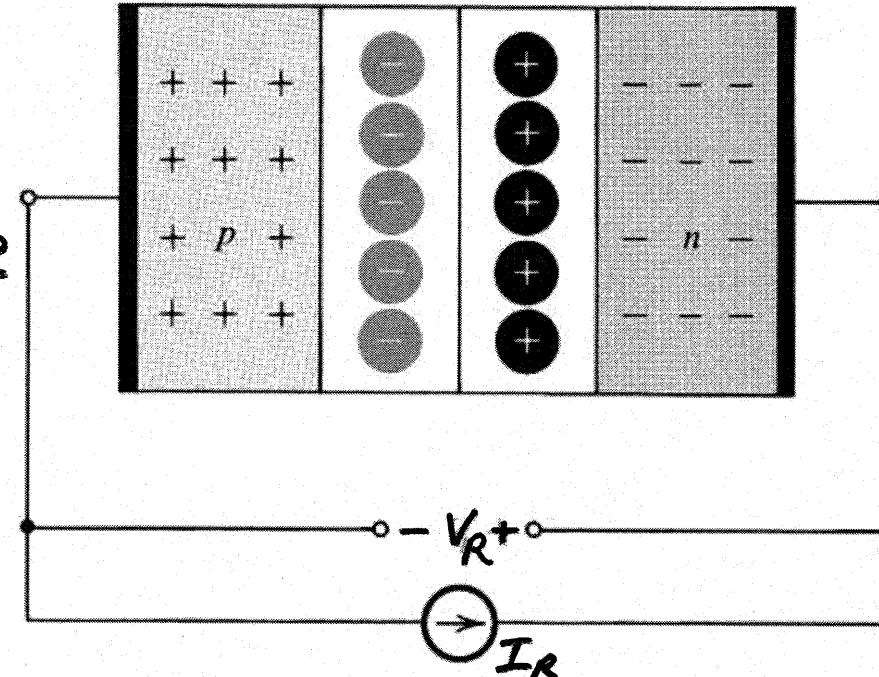
$$I_D \longrightarrow \xleftarrow{I_s}$$

Either:

Assume current source

$$I_R \ll I_s$$

\rightarrow see text treatment



Or: Reverse bias V_R adds to diffusion barrier V_0 and decreases equilibrium I_D

$$I_R = I_s - I_D$$

Figure 3.46 The pn junction excited by a constant-current source I in the reverse direction. To avoid breakdown, I is kept smaller than I_s . Note that the depletion layer widens and the barrier voltage increases by V_R volts, which appears between the terminals as a reverse voltage.

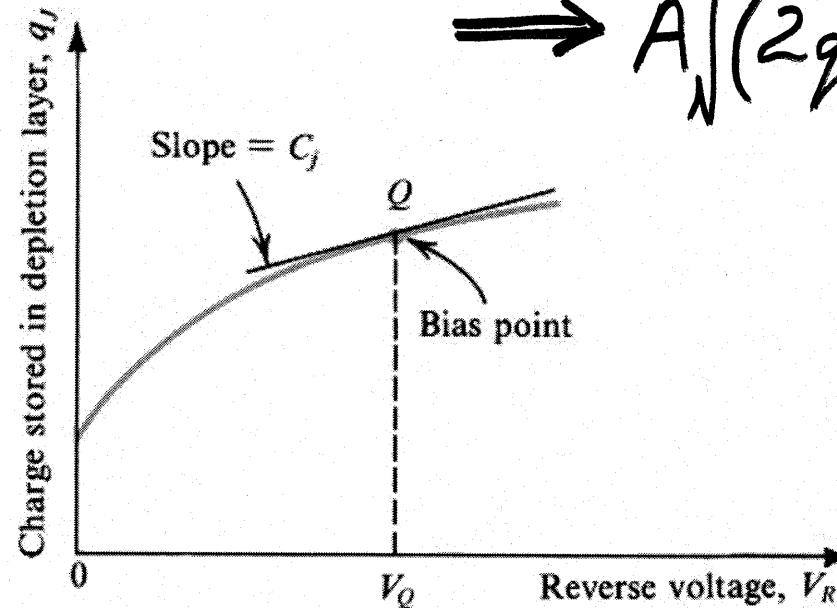
$$\Delta V_{depl} = \sqrt{\left(\frac{2\epsilon_{Si}}{q}\right)\left(\frac{1}{N_A} + \frac{1}{N_D}\right)(V_0 + V_R)}$$

Eventually $V_R \gg 0$, $I_D \rightarrow 0$, and $I_R \rightarrow I_s$

Depletion Capacitance → charge separation

$$q_J = q_N = q_P = q N_D x_n A = q N_A x_p A$$

$$\Rightarrow A \sqrt{\left(2q\epsilon_{Si}\right) \frac{N_A N_D}{N_A + N_D} (V_0 + V_R)}$$



Either : $C_J = \frac{\epsilon_{Si} A}{W_{depl}} = \frac{\epsilon_{Si} A}{\sqrt{(2\epsilon_{Si}/q) \left(\frac{N_A + N_D}{N_A N_D}\right) (V_0 + V_R)}} = A \left(\frac{\epsilon_{Si} q}{2} \cdot \frac{N_A N_D}{N_A + N_D}\right)^{1/2} (V_0 + V_R)^{-1/2}$

Or :
 Small signal Depletion Capacitance $C_J = \left. \frac{dq_J}{dV_R} \right|_{V_R=V_Q} = A \sqrt{\left(2q\epsilon_{Si}\right) \frac{N_A N_D}{N_A + N_D}} \cdot \frac{1}{2} \cdot (V_0 + V_R)^{-1/2}$ same

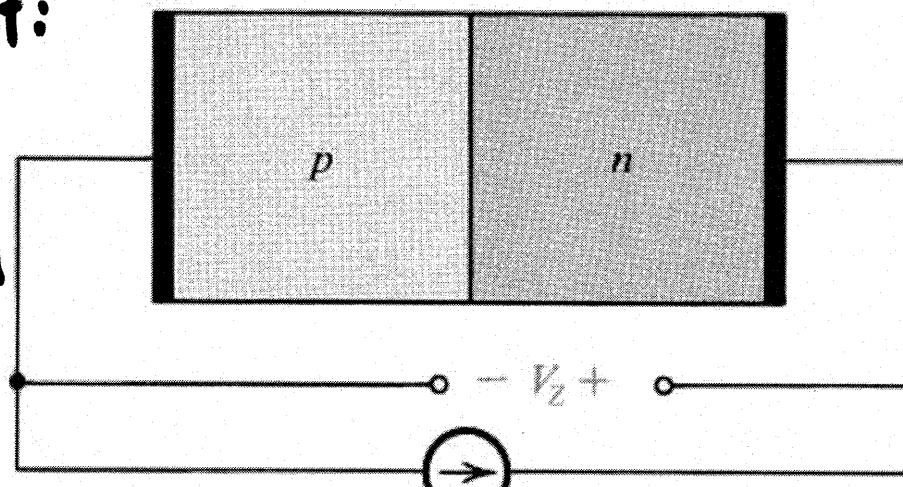
Write as $C_J = C_{J0} \frac{(V_0 + V_R)^{-1/2}}{V_0^{-1/2}} = \frac{C_{J0}}{(1 + V_R/V_0)^{1/2}} \rightarrow \frac{C_{J0}}{(1 + V_R/V_0)^m}$

$m = 1/2$ abrupt junction
 $m = 1/3$ linearly graded

Reverse Breakdown: if $V_R \xrightarrow{\text{increase}} V_{ZK}$

Zener Effect:

Electric field
in the depletion
region creates
electron-hole
pairs (by field ionization)



Avalanche Effect:

Electrons accelerated
in the depletion region
Electric field gives
sufficient energy
to create electron-hole pairs
(by impact ionization)
More carriers \rightarrow current
increases

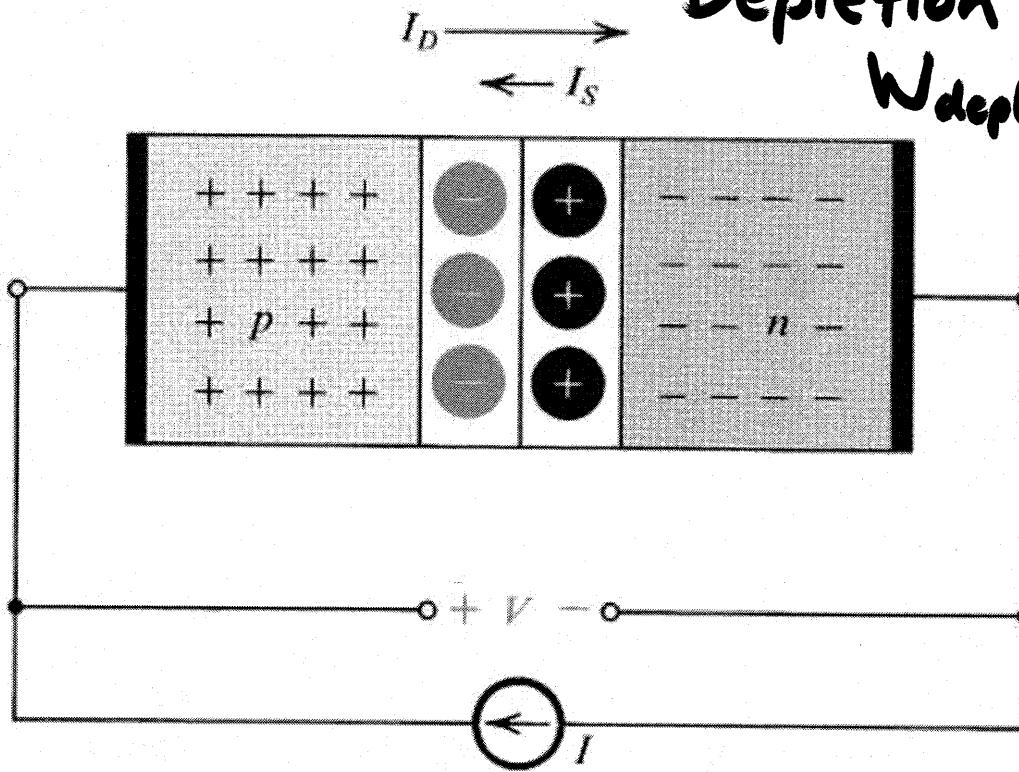
Figure 3.48 The pn junction excited by a reverse-current source I , where $I > I_S$. The junction breaks down, and a voltage V_Z , with the polarity indicated, develops across the junction.

Ex. 3.33

Junction capacitance

Forward Bias

$V_0 \rightarrow V_0 - V$, I_D incr
Depletion width decreases
 $W_{depl} \rightarrow (X(V_0 - V))^{1/2}$



Majority holes from P → cross depletion region → minority in N region
Majority electrons from N → cross depletion region → minority in P region & recombine with majority carriers

Figure 3.49 The pn junction excited by a constant-current source supplying a current I in the forward direction. The depletion layer narrows and the barrier voltage decreases by V volts, which appears as an external voltage in the forward direction.

Recombination requires replenishment from external circuit

side
+
is depletion
layer.

transistor
ish
recomb =

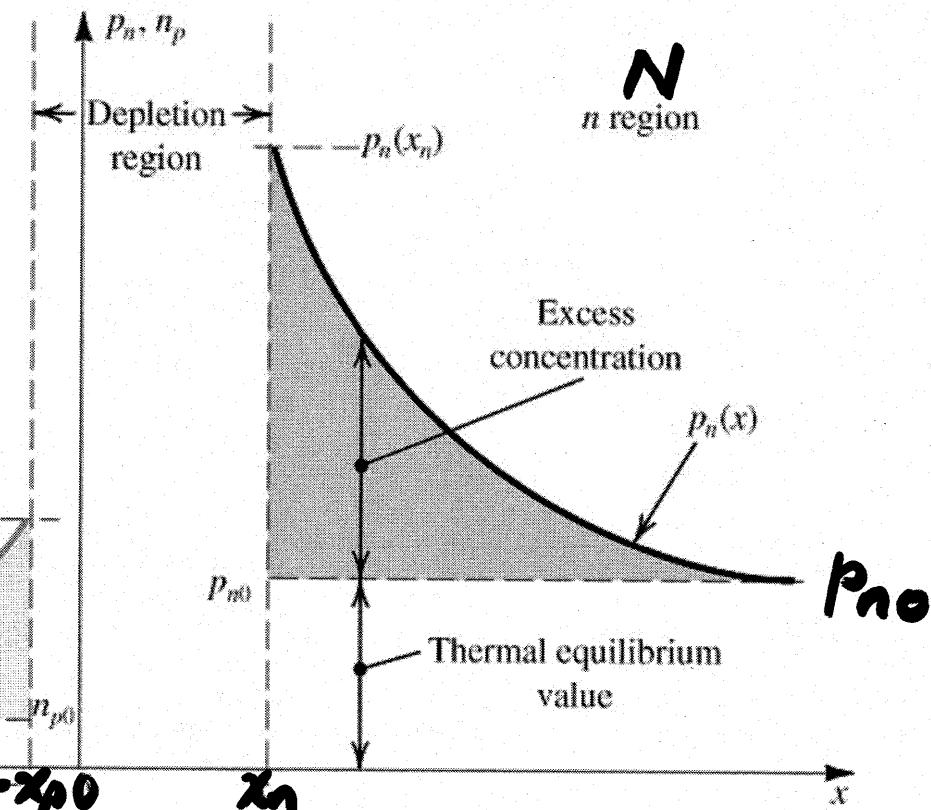
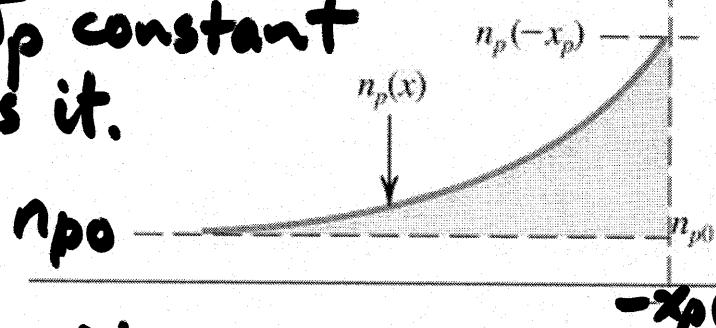
trans
external
unit

trans
Ckt

Minority Carrier Recombination

Note:

Some recombination
in space charge region,
but neglect, so
 J_n, J_p constant
across it.



Here $N_A > N_D \therefore n_{p0} < p_{no}$ & $x_p < x_n$
 $\bar{J}_{\text{diffusion}} = \bar{J}_{npl}(-x_p) + \bar{J}_{pnl}(x_n)$

Figure 3.50 Minority-carrier distribution in a forward-biased pn junction. It is assumed that the p region is more heavily doped than the n region; $N_A @ N_D$.

Carrier Recombination and Currents

$$p_n(x_n) = p_{n0} \exp(V/V_T) \quad \xrightarrow[V=0]{} p_{n0}$$

$$\& \quad p_n(x) = p_{n0} + [p_n(x_n) - p_{n0}] \exp - \frac{x-x_n}{L_p}$$

L_p = Minority carrier diffusion length of holes in N-type material
 $(\sim 1 \text{ to } 100 \mu\text{m}) = \sqrt{D_p \tau_p}$

Defines Minority Carrier Lifetime $\tau_p = L_p^2 / D_p$
 $(\sim 1 \text{ to } 10^4 \text{ ns})$

Diffusion $J_p = -q D_p \left. \frac{dp_n(x)}{dx} \right|_{x=x_n}$
 $= -[p_{n0} \exp \frac{V}{V_T} - p_{n0}] \left[\exp - \frac{x-x_n}{L_p} \right] \left(-\frac{1}{L_p} \right) q D_p$

$$J_p(x_n) = (q D_p / L_p) p_{n0} \left(\exp \frac{V}{V_T} - 1 \right)$$

Similarly $J_n(-x_p) = (q D_n / L_n) n_{p0} \left(\exp \frac{V}{V_T} - 1 \right)$

$$\& \quad J = J_p(x_n) + J_n(-x_p) \quad (= J_p(x) + J_n(x))$$

$$\begin{aligned} \text{So } J &= J_n + J_p \\ &= q \left(\frac{D_n}{L_n} n_{p0} + \frac{D_p}{L_p} p_{n0} \right) \left(\exp \frac{V}{V_F} - 1 \right) \end{aligned}$$

$$\begin{aligned} \rightarrow I &= A q n_i^2 \left(\frac{D_n}{L_n} \frac{1}{N_A} + \frac{D_p}{L_p} \frac{1}{N_D} \right) \left(\exp \frac{V}{V_F} - 1 \right) \\ &= I_s \left(\exp \frac{V}{V_F} - 1 \right) \end{aligned}$$

where

$$I_s = A q n_i^2 \left(\frac{L_n / \tau_n}{N_A} + \frac{L_p / \tau_p}{N_D} \right)$$

Strong T dependence

Diffusion Capacitance

$$C_D = dQ/dV = \tau_T (dI/dV)$$

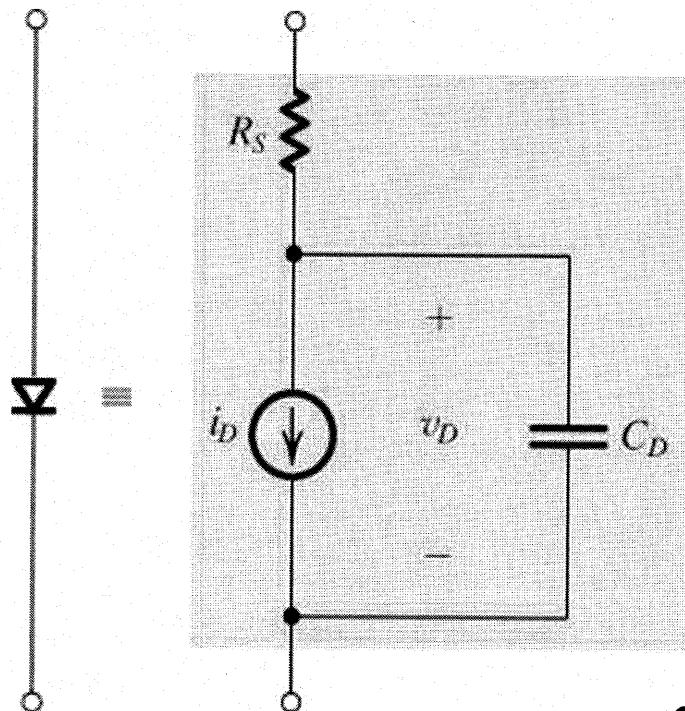
$$I = I_s (\exp \frac{V}{V_T} - 1)$$

$$\therefore \frac{dI}{dV} = \frac{I_s}{V_T} \exp \frac{V}{V_T} = \frac{I + I_s}{V_T} \approx \frac{I}{V_T}$$

$$\therefore C_D \approx \frac{\tau_T}{V_T} I \quad \xrightarrow{\text{for reverse bias}} 0$$

C_j depletion capacitance dominates for reverse bias
 C_D diffusion " " " forward "

Diffusion Capacitance & Spice Model



$$i_D = I_S (e^{v_D/nV_T} - 1)$$

$$C_D = C_d + C_j = \frac{T_f}{V_T} I_S e^{v_D/nV_T} + C_{j0} / \left(1 - \frac{v_D}{V_0}\right)^m$$

Depletion Capacitance

Diffusion Capacitance
(Excess minority carriers)

Excess stored charge $Q_p = \int_{x_n}^{\infty} [\bar{P}_n(x_n) - P_{n0}] \exp - \frac{x-x_n}{L_p} dx$

$$= Aq P_{n0} \left(\exp \frac{V}{V_T} - 1 \right) (-L_p)(0-1)$$

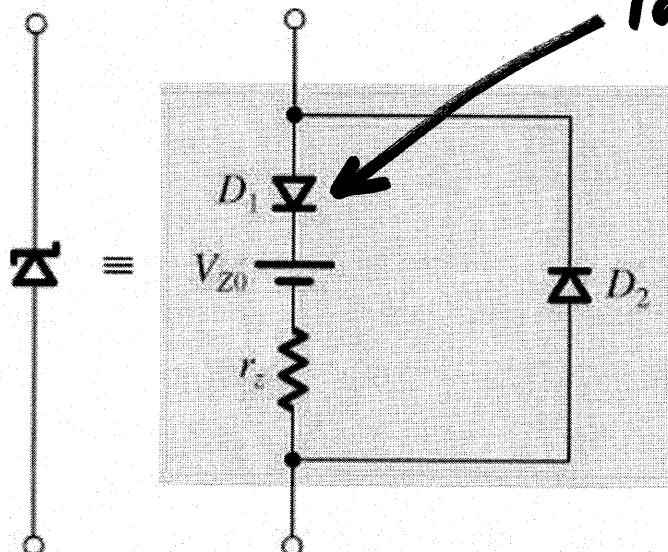
$$I_p = qA \frac{D_p}{L_p} P_{n0} \quad \rightarrow \quad = L_p^2 / D_p \cdot I_p = \tau_p I_p$$

$$\Delta Q_n = \tau_n I_n$$

$$\therefore Q = \tau_p I_p + \tau_n I_n \Rightarrow \tau_T I \quad \text{where } \tau_T = \text{mean transit time}$$

Figure 3.51 The SPICE diode model.

Spice Model : Zener Diode



Ideal: n very small
makes
 V_{DO} small

Figure 3.52 Equivalent-circuit model used to simulate the zener diode in SPICE. Diode D_1 is ideal and can be approximated in SPICE by using a very small value for n (say $n = 0.01$).

Check the Spice examples

PARAMETERS:

$$C = 520\mu$$

$$R = 191$$

$$R_{isolation} = 100E6$$

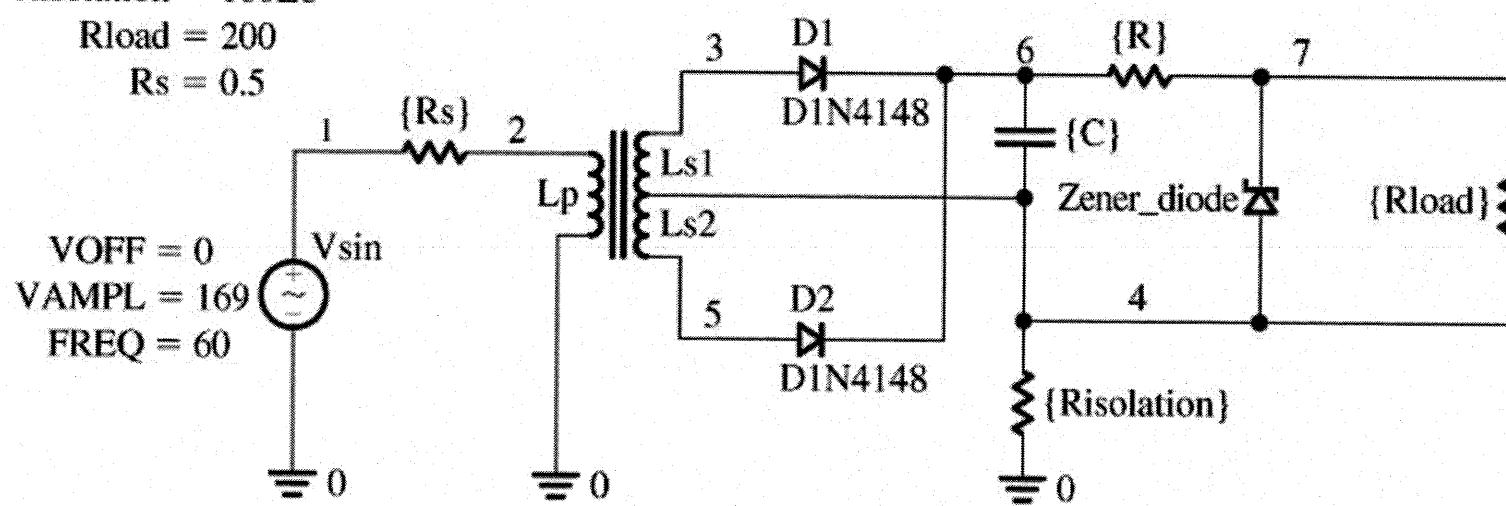
$$R_{load} = 200$$

$$R_s = 0.5$$

$$V_{OFF} = 0$$

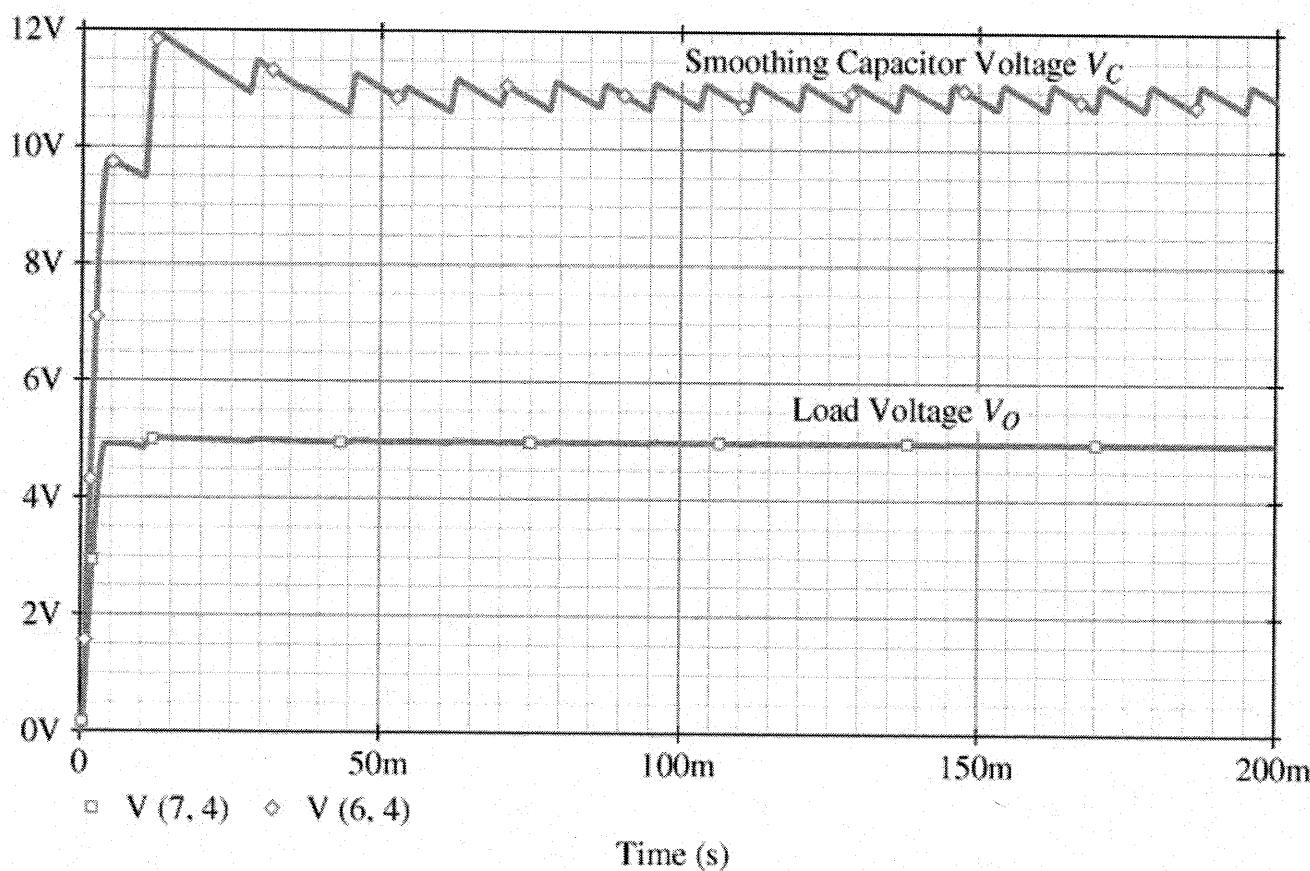
$$V_{AMPL} = 169$$

$$FREQ = 60$$



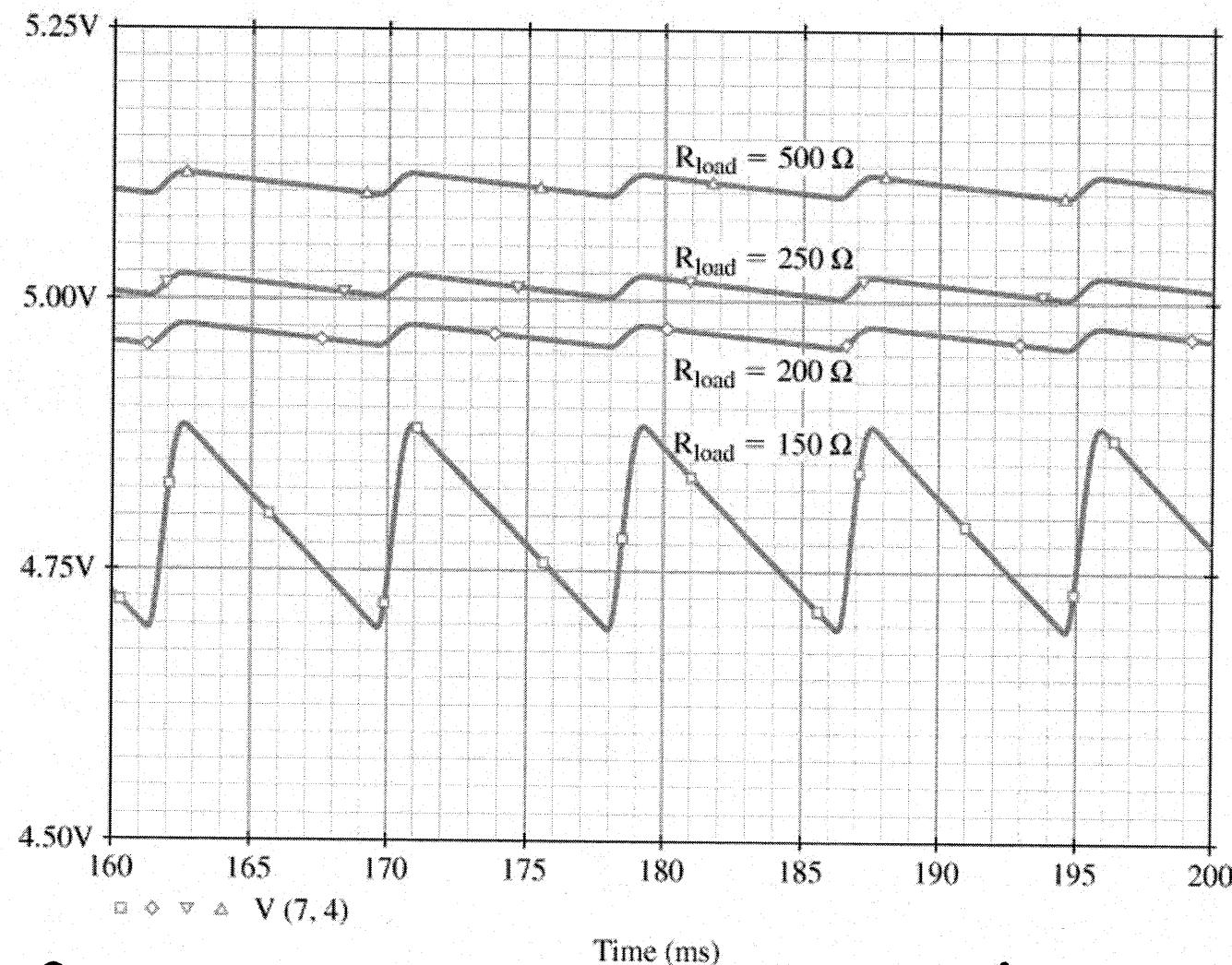
Full wave rectification + smoothing filter
+ zener regulator

Figure 3.53 Capture schematic of the 5-V dc power supply in Example 3.10.



Transient power supply response

Figure 3.54 The voltage v_C across the smoothing capacitor C and the voltage v_O across the load resistor $R_{\text{load}} = 200 \Omega$ in the 5-V power supply of Example 3.10.



Ripple variation with load

Figure 3.55 The output-voltage waveform from the 5-V power supply (in Example 3.10) for various load resistances: $R_{load} = 500 \Omega$, 250Ω , 200Ω , and 150Ω . The voltage regulation is lost at a load resistance of 150Ω .

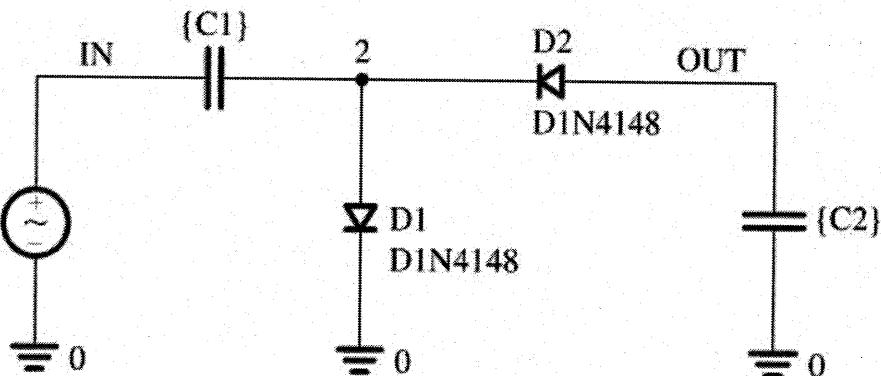
Voltage doubler

PARAMETERS:

C1 = 1u

C2 = 1u

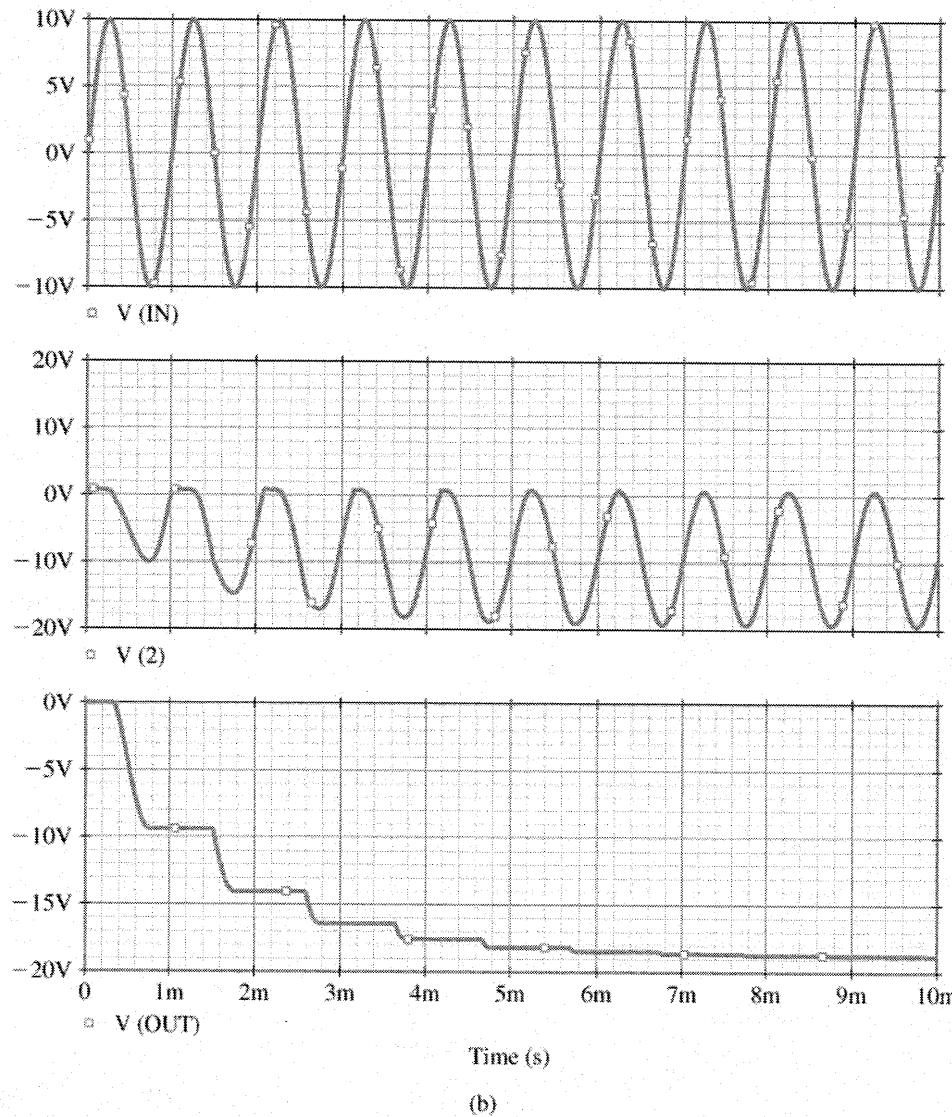
VOFF = 0
VAMPL = 10V
FREQ = 1K



(a)

Figure E3.35 (a) Capture schematic of the voltage-doubler circuit (in Exercise 3.35).

Doubler transient



(b)

$$V_P = 10\text{V}$$

$$V_{out} = -20\text{V}$$

Figure E3.35 (Continued) (b) Various voltage waveforms in the voltage-doubler circuit. The top graph displays the input sine-wave voltage signal, the middle graph displays the voltage across diode D_1 , and the bottom graph displays the voltage that appears at the output.

Ex 3.29 Calculate n_i for Si at 250K, 300K, 350K.

Either $n_i/\text{cc} = \sqrt{5.4 \times 10^{31} \cdot T^3 \cdot \exp - \frac{1.12 \times 1.6 \times 10^{-19}}{1.38 \times 10^{-23} T}}$

OR $n_i(300\text{K}) = 1.5 \times 10^{10}/\text{cc}$ $\therefore n_i(T) = (1.5 \times 10^{10}/\text{cc}) \left(\frac{T}{300}\right)^{3/2} \exp\left[\frac{-6493(1-\frac{300}{T})}{300}\right]$
 gives $n_i(350\text{K}) = 41.6 \times 10^{10}/\text{cc}$
 and $n_i(250\text{K}) = 0.015 \times 10^{10}/\text{cc}$

Ex 3.30 N type Si, $N_D = 10^{17}/\text{cc}$. Find n & p at 250K, 300K, 350K.

Temperature	$n_{N_D} = N_D$	n_i (above)	n_i^2	$p_{N_D} = n_i^2 / N_D$
250K	$10^{17}/\text{cc}$	1.5×10^8	2.25×10^{16}	$2.25 \times 10^{-1}/\text{cc}$
300K	$10^{17}/\text{cc}$	1.5×10^{10}	2.25×10^{20}	$2.25 \times 10^3/\text{cc}$
350K	$10^{17}/\text{cc}$	4.2×10^{11}	17.64×10^{22}	$1.76 \times 10^6/\text{cc}$

Ex 3.31 Find resistivities ρ of (a) intrinsic & (b) extrinsic Si (P type)

$$n_i = 1.5 \times 10^{10}/\text{cc} \quad \mu_n = 1350 \text{ cm}^2/\text{Vs} \quad \mu_p = 480 \text{ cm}^2/\text{Vs} \quad \text{for intrinsic}$$

$$N_A = 10^{16}/\text{cc} \quad \mu_n = 1110 \text{ cm}^2/\text{Vs} \quad \mu_p = 1100 \text{ cm}^2/\text{Vs} \quad \text{for extrinsic}$$

(a) Intrinsic $\rho = [1.6 \times 10^{-19} \cdot 1.5 \times 10^{10} (1350 + 480)]^{-1} = 2.28 \times 10^5 \Omega \cdot \text{cm}$

(b) Extrinsic $\rho = \frac{1}{q(n\mu_n + p\mu_p)} \quad n_p = n_i^2 / N_A = (1.5 \times 10^{10})^2 / 10^{16} \quad \therefore \rho = [1.6 \times 10^{-19} (2.25 \times 10^4 \times 1110 + 10^{16} \times 400)]^{-1}$
 $= 2.25 \times 10^4 \quad \& \quad p_p = N_A = 1.56 \Omega \cdot \text{cm}$

Ex 3.32 PN junction $N_A = 10^{17}/\text{cm}^3$ $N_D = 10^{16}/\text{cm}^3$

$$T = 300K$$

$$n_i = 1.5 \times 10^{10}/\text{cc}$$

Find V_0 , W_{depl} , x_p , x_n .

$$V_0 = V_T \ln \frac{N_A N_D}{n_i^2} = 25 \text{mV} \ln \frac{10^{17} 10^{16}}{2.25 \times 10^{20}} = 0.728 \text{V}$$

$$\begin{aligned} x_n &= \left(\frac{2e_{si}}{q} \frac{N_A/N_D}{N_A+N_D} V_0 \right)^{1/2} \\ &= \left[\frac{2 \times 1.04 \times 10^{-19} \times 0.728}{1.6 \times 10^{-19} \times 1.1 \times 10^{17}} \right]^{1/2} \sqrt{10} \\ &= 0.87 \sqrt{10} \times 10^{-5} \text{cm} \\ &= 0.27 \mu\text{m} \end{aligned}$$

$$\begin{aligned} x_p &= \left(\frac{2e_{si}}{q} \frac{N_D/N_A}{N_A+N_D} V_0 \right)^{1/2} \\ &= \left[\frac{2 \times 1.04 \times 10^{-19} \times 0.728}{1.6 \times 10^{-19} \times 1.1 \times 10^{17}} \right]^{1/2} \sqrt{10} \\ &= 1.087 \sqrt{10} \times 10^{-5} \text{cm} \\ &= 0.027 \mu\text{m} \end{aligned}$$

$$\therefore W_{\text{depl}} = 0.27 + 0.027 = 0.30 \mu\text{m}$$

OR find W_{depl} , then x_n & x_p

Ex 3.33 PN junction $N_A = 10^{17}/\text{cm}^3$ $N_D = 10^{16}/\text{cm}^3$ at 300K

Find (a) $C_{j0}/\mu\text{m}^2$ (b) C_j at reverse bias $V_R = 2V$
for junction area $2500\mu\text{m}^2$

Assume $n_i = 1.5 \times 10^{10}/\text{cc}$ $m = 1/2$ & $V_0 = 0.728V$ (Ex 3.32)

$$(a) C_{j0} = A \left(\frac{\epsilon_{Si} q}{2} \cdot \frac{N_A N_D}{N_A + N_D} \right)^{1/2} V_0^{-1/2} \rightarrow C_{j0}/A = 10^{-8} \left\{ \frac{1.6 \times 10^{-19}}{\frac{1.04 \times 10^{-12}}{\frac{10^{17} \times 10^{16}}{(2 \times 0.728 \times 1.1 \times 10^9)}}} \right\}^2$$

$$= 3.22 \times 10^{-16}/\mu\text{m}^2$$

$$= 0.322 \text{ fF}/\mu\text{m}^2$$

$$(b) \therefore C_j = \frac{C_{j0}}{\left(1 + \frac{2}{0.728}\right)^{1/2}} \times 2500 \text{ fF} = 415.85 \text{ fF}$$

$$= 0.42 \mu\text{F}$$