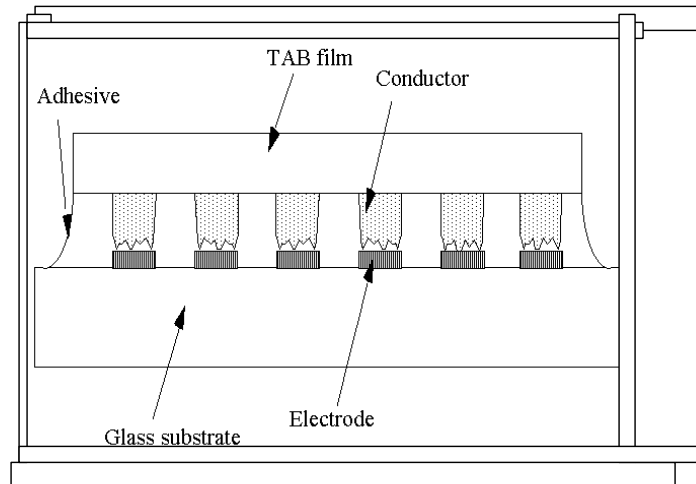


# NCA: Non-Conductive Adhesive



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## A.2 Technology Drivers

- **2.1 Environment**
  - **Environmental:**
    - no-flux, no-Pb
  - **No-Pb solders**
    - -Melting temperatures
    - -Thermomechanical stress
  - **Silver effects**
- **2.2 Economics**
  - **Manufacturing**
    - Fewer process steps
    - Available technologies (stencil/screen/dispense)
- **2.3 Technology drivers (c.f. solder)**
  - **Thermomechanical stress**
    - Low process temperature
    - High compliance
  - **Fine-pitch (area array) interconnect**
    - Smaller particles than solder
    - No slumping
    - Inter-metallic diffusion in solders
    - Electromigration

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## A.3. ECA Applications

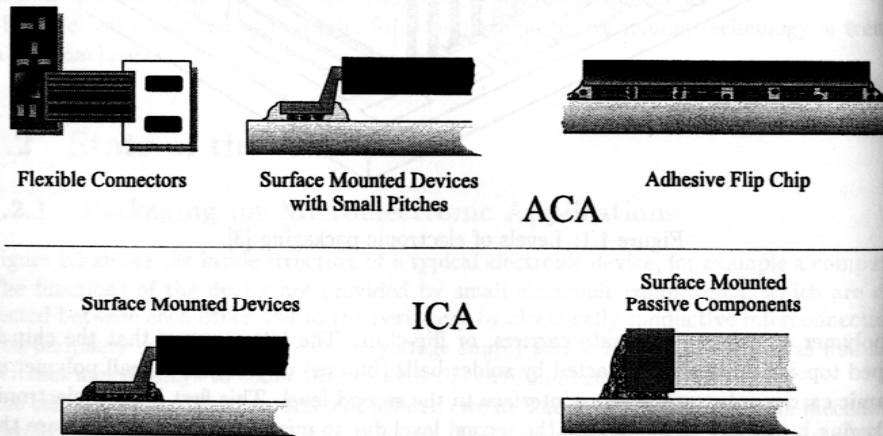
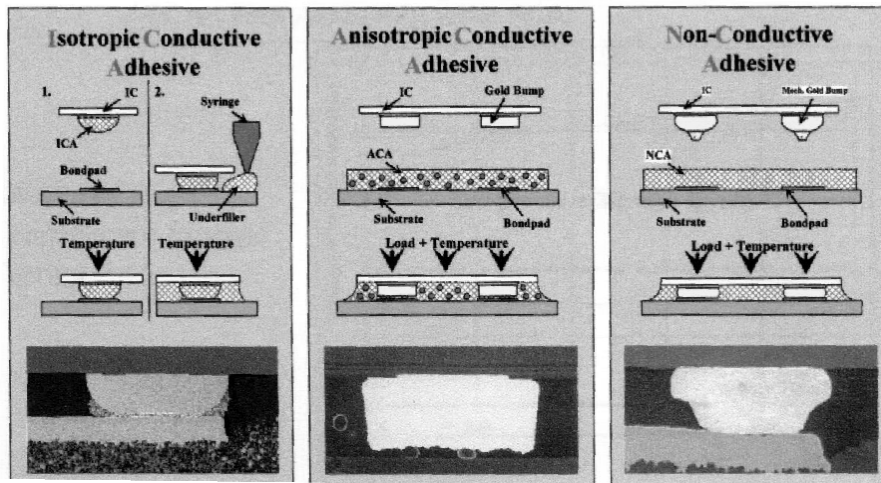


Figure 1.2: ECA fields of application.

## A.4. Processing e.g. Flip-Chip Assembly (IZM, Berlin)



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# A.5. Materials

## 5.1 Metals

- Nickel/noble metals
- Silver
  - Silver Oxide

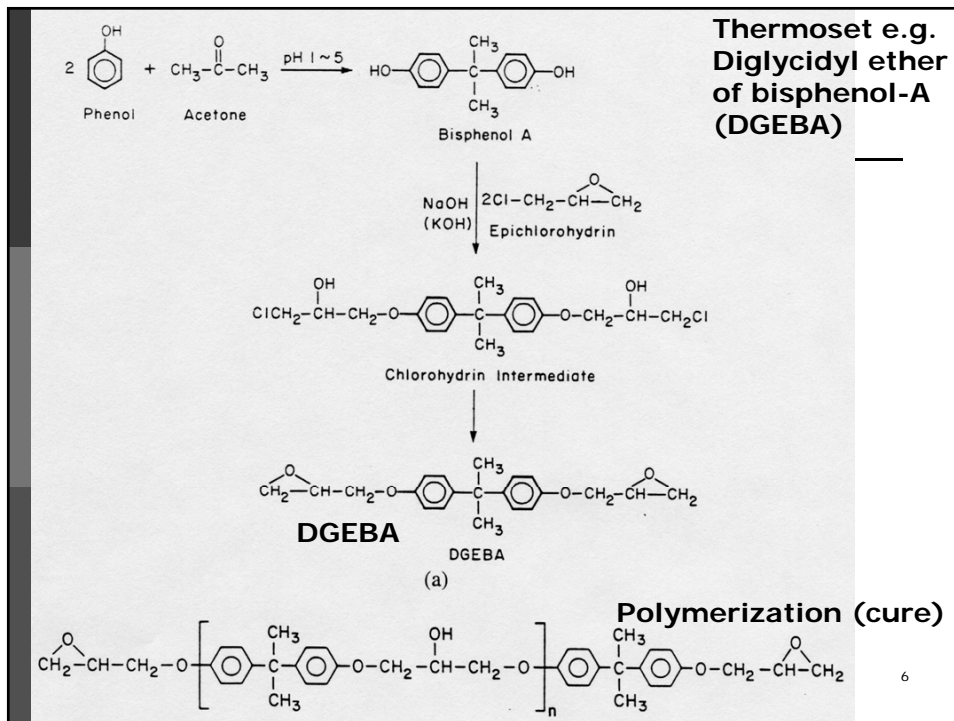
## 5.2 Polymers

- Thermoplastics - chains
- Thermoset epoxies -cross-link
- Thermoset/thermoplastic blends
- Additives
- Polyimide, silicones

## 5.3 Polymer Cure

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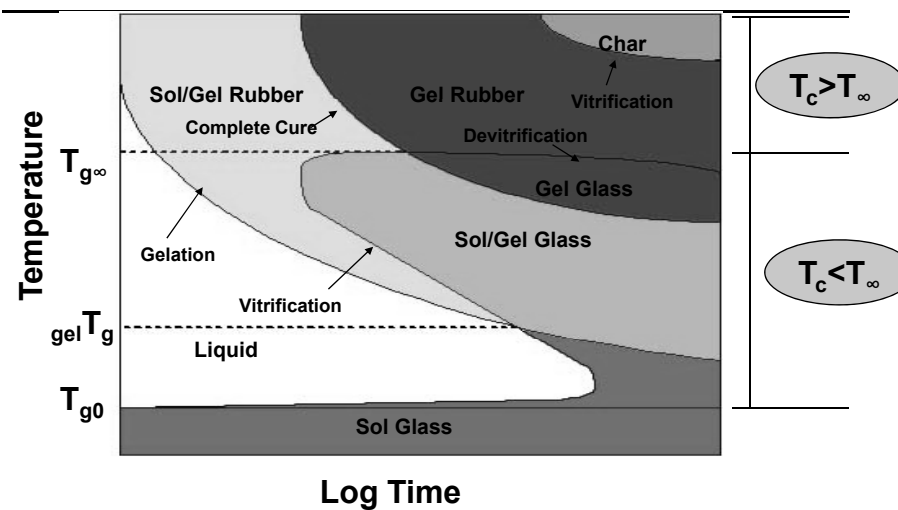
## A.5.3 Curing

- 5.3.1 Cure process
- 5.3.2 Cure modeling
- 5.3.3 Glass transition temperature  $T_g$
- 5.3.3 Cure optimization

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### A.5.3.1 Cure Process



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## Cure Effects

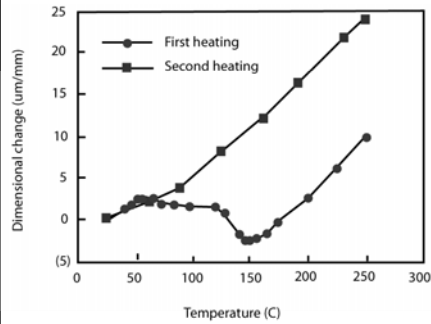


Figure 1. Dimensional change of conductive adhesive

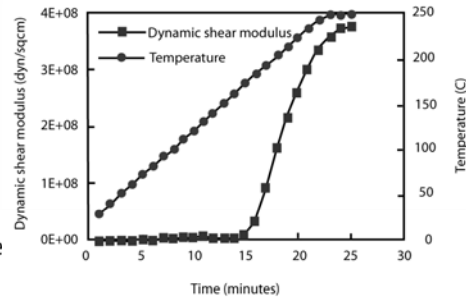


Figure 2. Dynamic shear modulus of conductive adhesive during cure

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## A.5.3.2 Cure Models

- Reaction rate  $d\alpha/dt = k f(\alpha)$ ,  
 where  $k = A \exp(-E/kT)$ 
  - $k$  = chemical rate constant,  $f(\alpha)$  reactant concn.
  - $\alpha$  = degree of cure
- N-th order model:  $f(\alpha) = (1 - \alpha)^n$
- Calculate degree of cure:
  - 1st order:  $d\alpha/dt = k(1 - \alpha)$ ,  $\therefore \alpha = 1 - \exp(-kt)$
  - 2nd order:  $d\alpha/dt = k(1 - \alpha)^2$ ,  $\alpha = 1 - (1 + kt)^{-1}$
- Auto-catalyzed model:
  - $f(\alpha) = \alpha^m (1 - \alpha)^n$
  - Linear combination:  $d\alpha/dt = k f(\alpha) = (k_1 + k_2 \alpha^m)(1 - \alpha)^n$

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## DSC: Directly determine degree of cure $\alpha$ and rate of cure $d\alpha/dt$

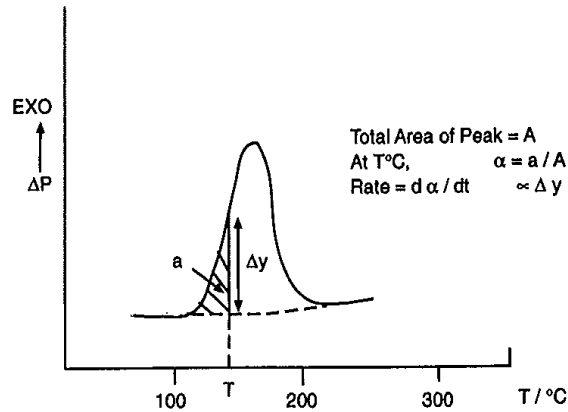


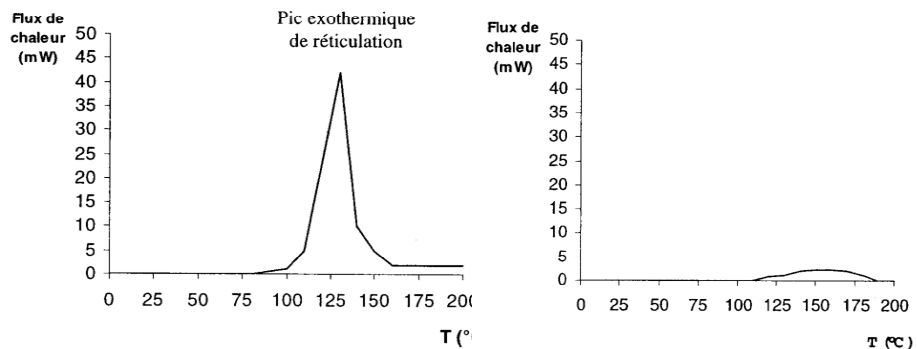
Figure 3.33 DSC curve for exothermic reaction showing measurement of partial and total areas.

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## Complete Cure: DSC before & after cure More accurate cure assessment

(Perichaud/Fremont)

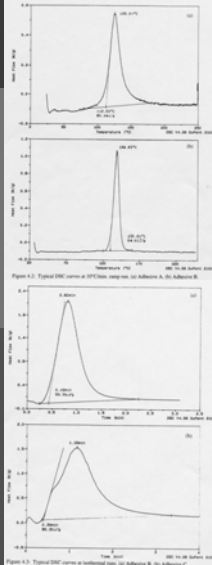


Use second DSC as measure of degree of cure -  $\int_1 HdT / (\int_1 HdT + \int_2 HdT)$

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## Cure Calculations: Differential Scanning Calorimetry (DSC) Heat flow vs time



$$\frac{d\alpha}{dt} = f(\alpha) \cdot A \cdot e^{-E/kT}, \text{ so } \int_0^{\alpha_p} \frac{1}{f(\alpha)} d(\alpha) = A \int_{T_0}^{T_p} e^{-E/RT} dt$$

$$= \left(\frac{A}{\phi}\right) \cdot \int_{T_0}^{T_p} e^{-E/RT} dT, \text{ if } T(t) = \phi t$$

$$\approx \left(\frac{A}{\phi}\right) \cdot \int_0^{T_p} e^{-E/RT} dT, \text{ if } T_0 \ll T_p$$

$$\approx \left(\frac{AE}{\phi R}\right) \cdot p\left(\frac{E}{RT_p}\right) \text{ where}$$

$$\log p(E/RT_p) \approx -2.315 - 0.4567E/RT_p$$

$$\text{for } 20 < \frac{E}{RT_p} < 60$$

Find:  $E \approx -\left(\frac{R}{0.4567}\right) \cdot \left(\frac{\Delta \log \phi}{\Delta(1/T_p)}\right)$

ie var'n of peak exothermic temp with heat rate, and

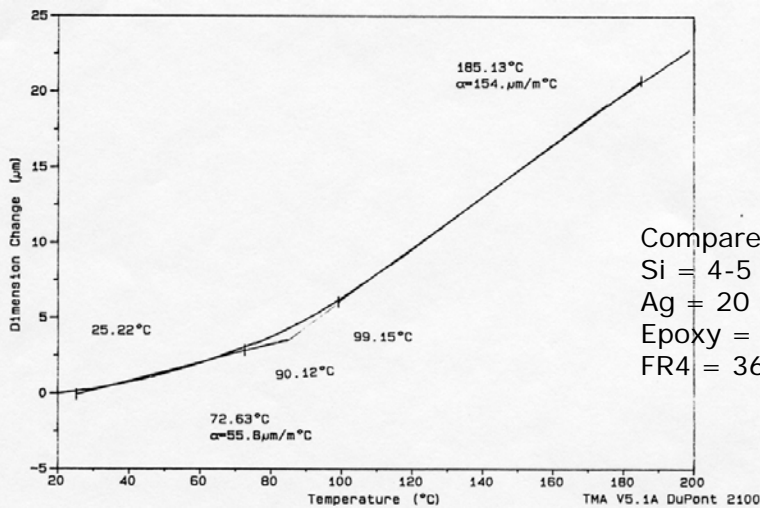
$$A = \left(\frac{\phi E}{RT_p^2}\right) e^{E/RT_p}$$

- k found for each T from E, A (experimental)
- E, A found from DSC, <sup>13</sup> heating rates

### A.5.3.3 Glass Transition Temperature

Table 4.3. TMA experimental results for cured block samples.

Materials	T <sub>g</sub> (°C)	CTE (<T <sub>g</sub> ) (μm/m°C)	CTE (>T <sub>g</sub> ) (μm/m°C)
Adhesive A	90	56	155
Adhesive B	90	61	168
Adhesive C	90	78	218

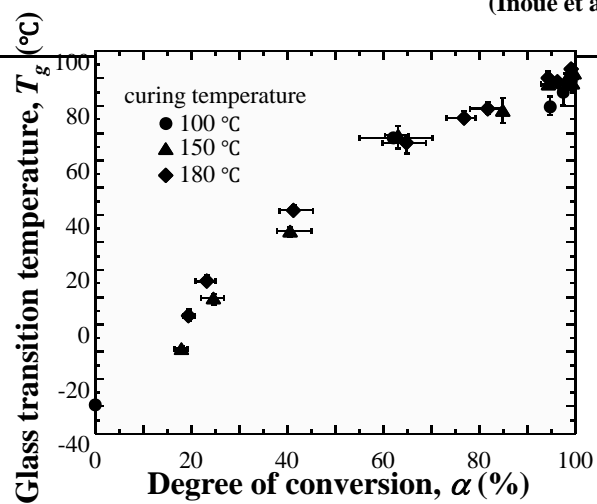


Compare CTEs:  
Si = 4-5 ppm/°C  
Ag = 20 ppm/°C  
Epoxy = 54 ppm/°C  
FR4 = 36 ppm/°C

Figure 4.4: Typical TMA graphs for Adhesive A showing CTE above and below T<sub>g</sub>.

## Relationship between degree of conversion and $T_g$

(Inoue et al)



One-to-one relationship between  $T_g$  and degree of conversion