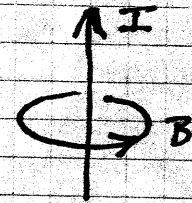


ECE 241 LECTURE 14 MAGNETIC FIELDS & CIRCUITS

MAGNETIC FIELDS

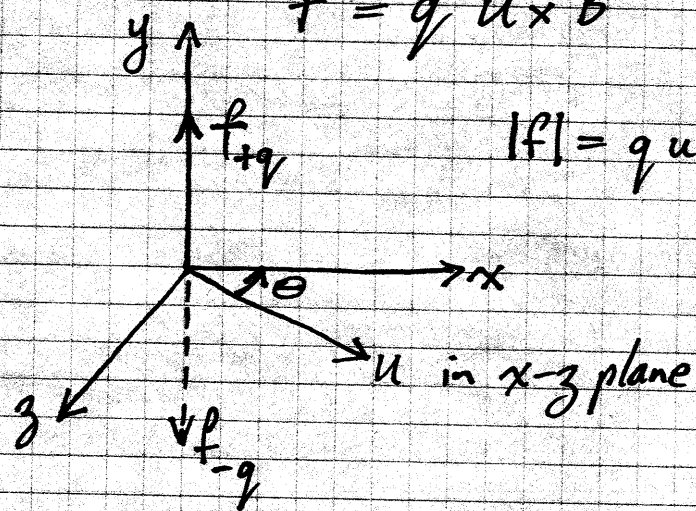
Moving charge \rightarrow magnetic field



Moving charge in magnetic field experiences force \rightarrow used to define magnetic field units

$$\vec{F} = q \vec{u} \times \vec{B}$$

Charge 1 C moving 1 m/s in field 1 Tesla (1 T) experiences force 1 N



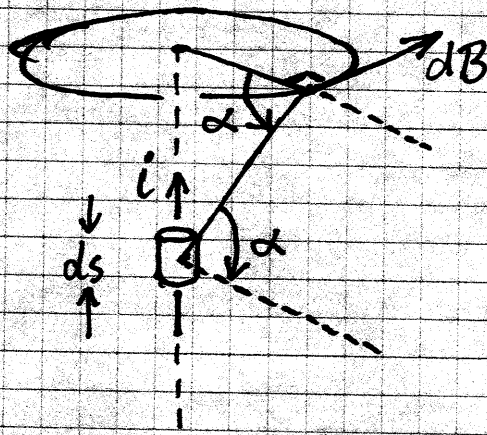
$$|\vec{F}| = q u B \sin \theta$$

Magnetic Flux $\phi = \int \vec{B} \cdot d\vec{A}$
(webers) \uparrow
magnetic field (Teslas)

Represent magnetic flux density by lines
(lines of magnetic force.) Tangents to
flux density vector \vec{B} .

Flux entering any closed surface = flux leaving, i.e. $\oint \vec{B} \cdot d\vec{A} = 0$

FIELD DUE TO CURRENT



dB due to element ds carrying current i

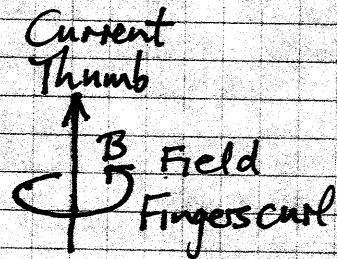
$$i = \frac{dq}{dt} \quad dq \text{ moves } ds \text{ in time } dt$$

$$\therefore u = \frac{ds}{dt}$$

$$\therefore i ds = \frac{dq}{dt} \cdot (u dt) = u dq$$

$$dB = \mu \frac{i ds \cos \alpha}{4\pi r^2}$$

RH Rule



$\mu = \text{permeability}$
 $= \mu_r \mu_0$
 μ_r relative permeability
 μ_0 freespace
 (units Wb/A-m or H/m)

MAGNETIC FIELD INTENSITY $\vec{H} = \frac{\vec{B}}{\mu}$ in A/m $\mu_0 = 4\pi \times 10^{-7} \text{ H/m}$

\vec{H} is "tendency" of moving charge to produce a field
 \vec{B} is the field actually produced, which depends on medium
 eg. higher in ferromagnetic materials high μ_r

FERROMAGNETISM

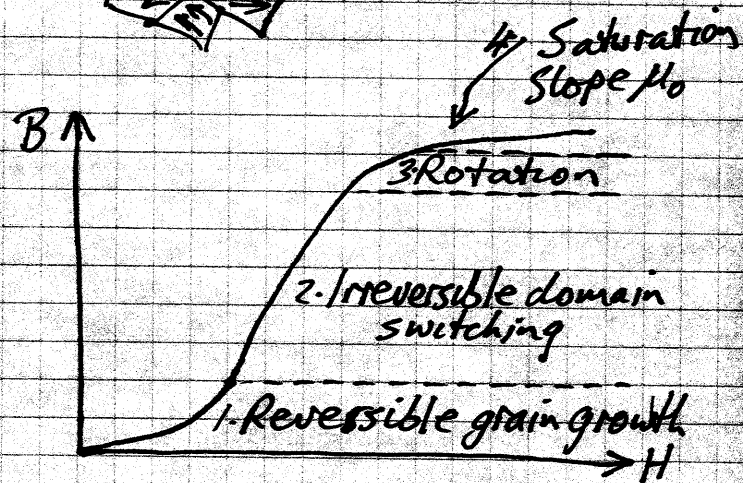
Magnetic domains \rightarrow aligned electron spins

Randomly oriented \rightarrow no external field



Apply external field to align domains

1. ~ Aligned domains grow
2. Misaligned domains switch polarization
3. Domain orientations rotate
4. Eventually all domains aligned \rightarrow saturation



$$\vec{B} = \mu_0 (\vec{H} + \vec{M}) \rightarrow \mu_0 \left(1 + \frac{\vec{M}}{\vec{H}}\right) \vec{H} = \mu_0 \mu_r \vec{H} = \mu \vec{H}$$

\uparrow Applied field intensity
 \uparrow Magnetic Polarization

μ_r not constant
Often assumed \sim constant.

LONG STRAIGHT CONDUCTOR

$$dB = \frac{\mu i ds \cos \alpha}{4\pi r^2}$$

$$\therefore B = \frac{\mu i}{4\pi} \int_{-\infty}^{\infty} \frac{\cos \alpha}{r^2} ds$$

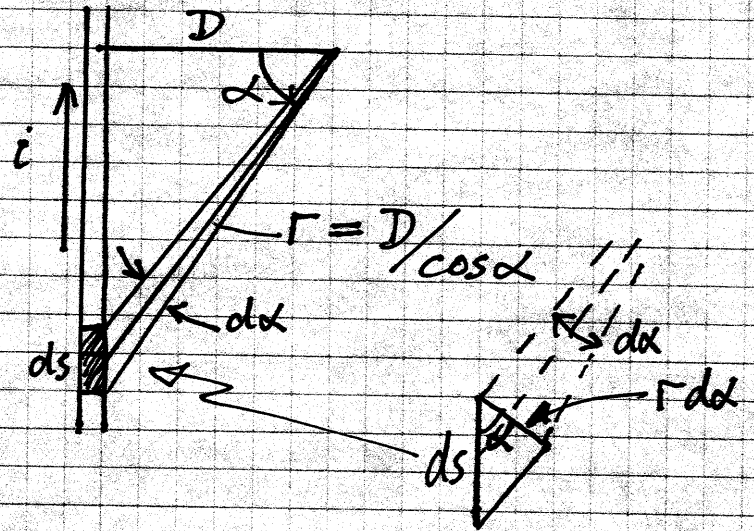
$$= \frac{\mu i}{4\pi D} \int_{-\pi/2}^{\pi/2} \cos \alpha d\alpha$$

$$= \frac{\mu i}{4\pi D} [\sin \alpha]_{-\pi/2}^{\pi/2} = \frac{\mu i}{4\pi D} [1 - (-1)] = \frac{\mu i}{2\pi D}$$

Note also: $\oint \vec{H} \cdot d\vec{l} = \oint \frac{B}{\mu} dl = \frac{i}{2\pi D} \cdot \oint dl = \frac{i}{2\pi D} \cdot 2\pi D = i$
 around closed loop radius D

$\int H \cdot dl =$ magnetomotive force
 (mmf)

Similar effect in magnetic circuits
 to emf in electric circuits.

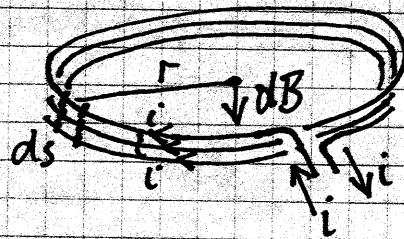


$$ds \cos \alpha = r dx$$

$$\frac{ds \cos \alpha}{r^2} = \frac{r dx}{r^2} = \frac{dx}{r} = \frac{\cos \alpha dx}{D}$$

Line integral of field intensity \vec{H} along any closed path
 = current linked by the path.

COIL FLUX DENSITY



B at center of flat coil, N-turns

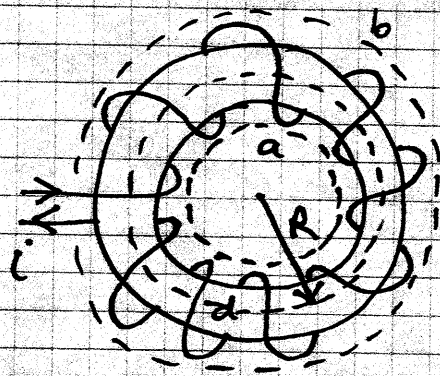
$$dB = \frac{\mu i ds \cos \alpha}{4\pi r^2} \xrightarrow[\cos \alpha = 1]{\alpha = 0} \frac{\mu i ds}{4\pi r^2}$$

$$B \text{ for one turn} = \int dB = \frac{\mu i}{4\pi r^2} \int_0^{2\pi r} ds = \frac{\mu i}{2r}$$

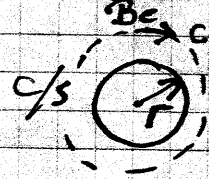
$$B \text{ for } N \text{ turns} = \frac{\mu N i}{2r}$$

eg. Exercise 20.2 10 turn coil, $r = 10 \text{ cm}$, $i = 0.1 \text{ A} \rightarrow B = \frac{4\pi \times 10^{-7} \times 10 \times 0.1}{2 \times 10^{-1}} = 2\pi \mu\text{T}$

TOROID FLUX DENSITY



Paths a, b, c, d as shown.



Path a links no current. $\therefore \int H dl = 0$
 $\therefore \vec{H}_a = 0$

Path b links no current (net current in = 0)
 $\therefore \vec{H}_b = 0$

Path c links i $\therefore \int H dl = i$ \therefore Find H around toroid, into center

Path d links i N times

$$\therefore \oint \vec{H} \cdot d\vec{l} = H \cdot 2\pi R = Ni \text{ Amp-turns}$$

$$B = \mu H = \frac{\mu N i}{2\pi R}$$

approx
 For uniform flux density in core ($r \ll R$)
 $\Phi = BA = \frac{\mu N i}{2\pi R} \pi r^2 = \frac{\mu N i r^2}{2R}$

Note: Flux $\phi = \mu \frac{\pi r^2}{2\pi R} Ni = \mu \frac{A}{l} F \leftarrow$ Basis of magnetic circuit

Magnetic field summary: $\vec{f} = q\vec{u} \times \vec{B}$

$$\phi = \int \vec{B} \cdot d\vec{A}$$

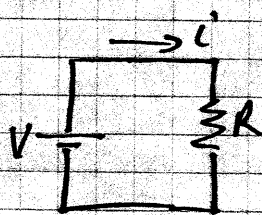
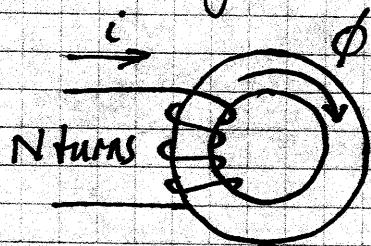
$$\vec{B} = \mu \vec{H}$$

$$dB = \frac{\mu i ds \cos \theta}{4\pi r^2}$$

$$\oint \vec{B} \cdot d\vec{A} = 0$$

$$\oint \vec{H} \cdot d\vec{l} = Ni$$

MAGNETIC CIRCUITS



Toroid:

Showed $\phi = BA = \mu Ni \frac{\pi r^2}{2\pi R} = \mu \frac{A}{l} F$

(above)

$F = Ni$ — mmf
magnetomotive force

ie. $\frac{F}{\phi} = \frac{1}{\mu} \frac{l}{A} = R$ (reluctance)
Amp-turns/Wb

Compare $\frac{V}{I} = \frac{1}{\sigma} \frac{l}{A} = R$

Analogous:

Electric

Magnetic

Current density \vec{J}
Current I
Electric field intensity \vec{E}
Voltage (emf) V
Conductivity σ
Resistance R

Magnetic Flux density \vec{B}
Magnetic flux ϕ
Magnetic field intensity \vec{H}
Magnetomotive force F
Permeability μ
Reluctance R

$$El = V = IR = \frac{J}{\sigma} l$$

$$Hl = F = \phi R = \frac{B}{\mu} l$$

Exercise 20.4: To establish flux 0.5 mWb in a toroidal iron core with 400 turns and $\mu_r = 1000$, c/s area $= 10^{-3} \text{ m}^2$ & $R = 0.04 \text{ m}$, find reluctance \mathcal{R} , mmf, and current required.

$$\text{Reluctance } \mathcal{R} = \frac{1}{\mu} \frac{l}{A} = \frac{1}{10^3 \times 4\pi \times 10^{-7}} \cdot \frac{2\pi(0.04)}{10^{-3}} = 2 \times 10^5 \text{ A.t/Wb}$$

↑ turns

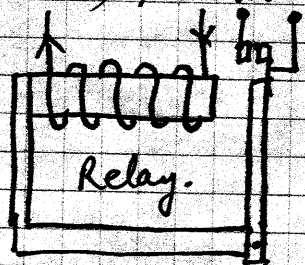
$$\mu = \mu_r \mu_0$$

$$F_{\text{mmf}} = \mathcal{R} \phi = 2 \times 10^5 \text{ A.t/Wb} \times 0.5 \times 10^{-3} \text{ Wb} = 100 \text{ A.t}$$

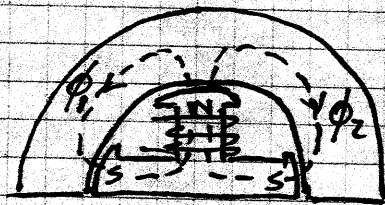
$$\therefore i = \frac{F}{N} = \frac{100 \text{ A.t}}{400 \text{ t}} = 0.25 \text{ A}$$

Where there is a winding on a high permeability material, flux is largely confined to (or concentrated in) that material.

Examples



Magnetic path around loop, across gap.



1/4 4-pole generator

Flux concentrated in ferromagnetic (iron) core --- plus air gap.

By analogy with electric circuits:

Series elements: $\phi = \phi_1 = \phi_2 = \phi_3 = \dots = \phi_n$

$$F = F_1 + F_2 + F_3 + \dots + F_n$$

Parallel elements: $\phi = \phi_1 + \phi_2 + \phi_3 + \dots + \phi_n$

$$F = F_1 = F_2 = F_3 = \dots = F_n$$

SERIES MAGNETIC CIRCUITS

Determine flux density

$B = \Phi/A$ in each element & corresponding field intensity $H = B/\mu$

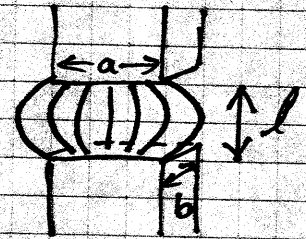
Calculate the mmf drop $F = H \cdot l$ for each element

Calculate total mmf = Ni and required current.

Air gap: $\mu \rightarrow \mu_0$ in air Account for fringing

1. Assume constant area \rightarrow increases mmf due to gap

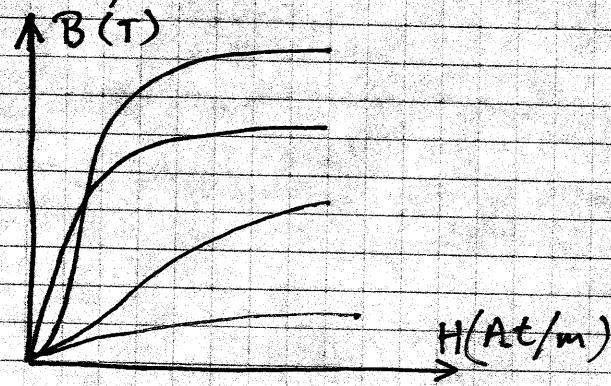
2. Account for fringing \rightarrow effective c/s area = $(a+l) \times (b+l)$



Find μ_r from magnetization curves

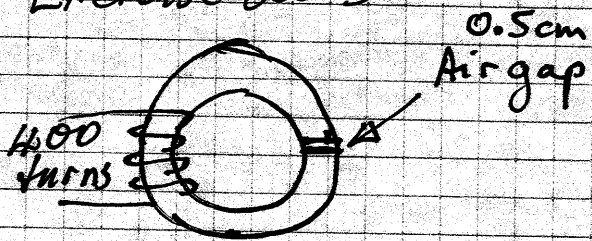
OR can often neglect R_{ferro}

since the air gap dominates R .



See Examples 4 & 5. \leftarrow Show that error in neglecting $R_{\text{ferro}} \sim 2.5\%$

Exercise 20-5



$$R = 0.04 \text{ m}$$

$$\frac{1}{2} \text{ area} = \pi r^2 = 10^{-3} \text{ m}^2$$

$$\phi = 10^{-3} \text{ Wb}$$

$$\mu_r = 1000$$

Determine R_{tot} & i for $\phi = 10^{-3} \text{ Wb}$

Account for fringing.

$$R = \frac{1}{\mu_r \mu_0} \frac{2\pi R - 5 \times 10^{-3}}{A} + \frac{1}{\mu_0} \frac{5 \times 10^{-3}}{A_{\text{air}}}$$

Rect-core: $(a+l)(b+l)$

$$= ab + (a+b)l + l^2$$

$A = 10^{-3} \text{ m}^2$ $a = ?$ $25 \times 10^{-6} \text{ m}^2$
 $b = ?$

Circular core: $\pi r^2 = 10^{-3} \text{ m}^2$

$$r = (10^{-3}/\pi)^{1/2} = 0.018 \text{ m}$$

\therefore effective diameter = $2 \times 0.018 + 0.005$
 $= 0.043 \text{ m}$

\therefore effective area for fringing
 $= \pi (0.0215)^2$

$\rightarrow 5 \times 10^{-3}$

$$R = \frac{2\pi(0.04)}{10^3 \mu_0 \times 10^{-3}} + \frac{1}{\mu_0} \frac{5 \times 10^{-3}}{\pi (0.0215)^2}$$

$$= 2 \times 10^5 + 2.74 \times 10^5 = 2.94 \times 10^6 \text{ A.t/Wb}$$

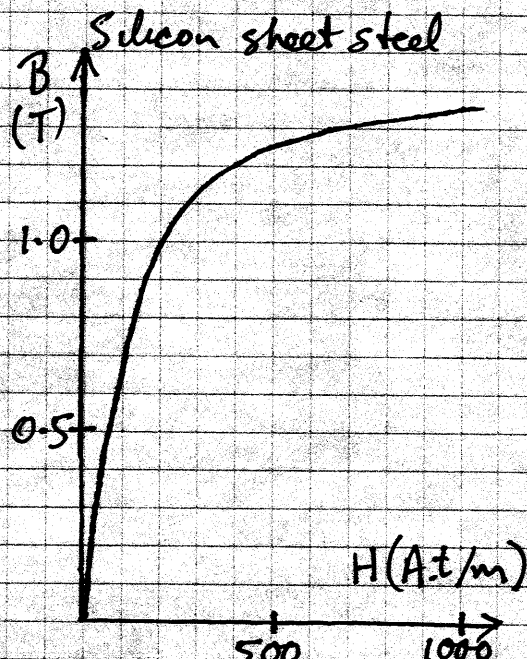
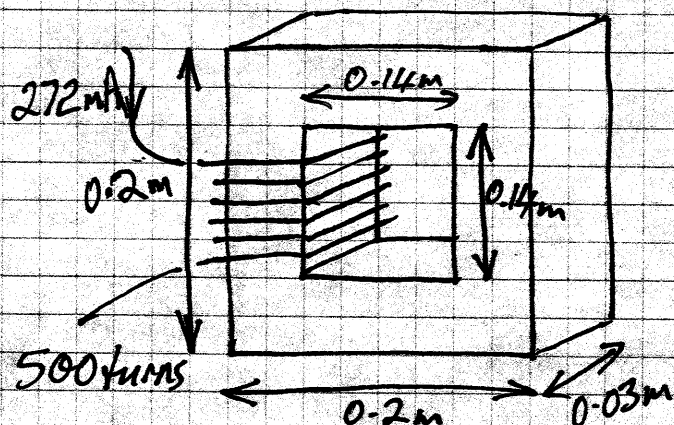
$\therefore F = Ni = \phi R = 2.94 \times 10^3 \text{ A.t}$

$\therefore i = \frac{F}{N} = \frac{2.94 \times 10^3}{400} = 7.35 \text{ A}$

(Different answers in dept)

Exercise 20.6

Use Fig 20.16 to find (a) H (b) B (c) ϕ



$$(a) \mathcal{F} = Ni = 500 \times 272 \times 10^{-3} = 136 \text{ A.t}$$

Core length:

Take central path

$$4 \times (0.14 + 0.03) = 0.68 \text{ m}$$

$$\mathcal{F} = Hl \therefore H = \frac{\mathcal{F}}{l}$$

$$= \frac{136 \text{ A.t}}{0.68 \text{ m}}$$

$$= 200 \text{ A.t/m}$$

(b) For $H = 200 \text{ A.t/m}$, $B = 1 \text{ T}$ (from the graph)

$$(c) \phi = B.A = 1 \text{ T} \times (0.03)^2 = 9 \times 10^{-4} = 0.9 \text{ mWb}$$

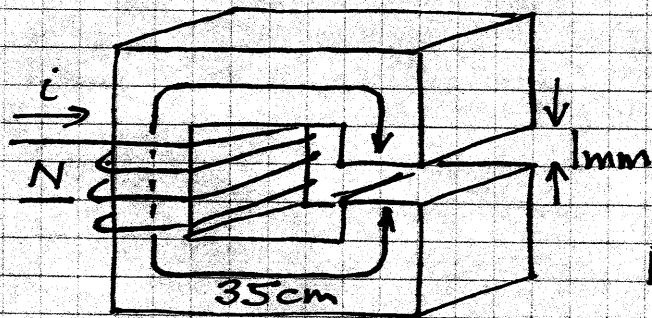
Exercise 20.7

Introduce 3 mm air gap & estimate flux density B for $i = 5.3 \text{ A}$

Assume all reluctance (mmf drop) in air gap

$$\therefore B = \mu \frac{Ni}{l} = \frac{4\pi \times 10^{-7} \cdot 500 \times 5.3}{3 \times 10^{-3}} = 1.11 \text{ T}$$

Example 6



Cast steel core

$$c/s \text{ area} = 10 \text{ cm}^2$$

$$N = 200 \text{ turns}$$

$$i = 3 \text{ A}$$

Find ϕ across gap

First assume all \mathcal{R} in gap.

$$B = \mu H = \frac{\mu_0 F}{l} = \frac{\mu_0 Ni}{l}$$

$$= \frac{4\pi \times 10^{-7} \times 200 \times 3}{10^{-3}}$$

$$= 0.754 \text{ T}$$

Note: fringing has been ignored.

More accurately —

See example: guess 0.6 T since $\mathcal{R}_{\text{core}}$ reduces B.

Read H from Fig 20.16 curve for cast steel

$$H = 400 \text{ A.t/m} \quad \therefore (Hl)_{\text{core}} = 400 \times 35 \times 10^{-2} = 140 \text{ A.t}$$

$$\& (Hl)_{\text{gap}} = \frac{(B l)_{\text{gap}}}{\mu_0} = \frac{10^{-3} \times 0.6}{4\pi \times 10^{-7}} = 478 \text{ A.t}$$

$$\therefore \text{Total mmf required} = 140 + 478 = 618 \text{ A.t}$$

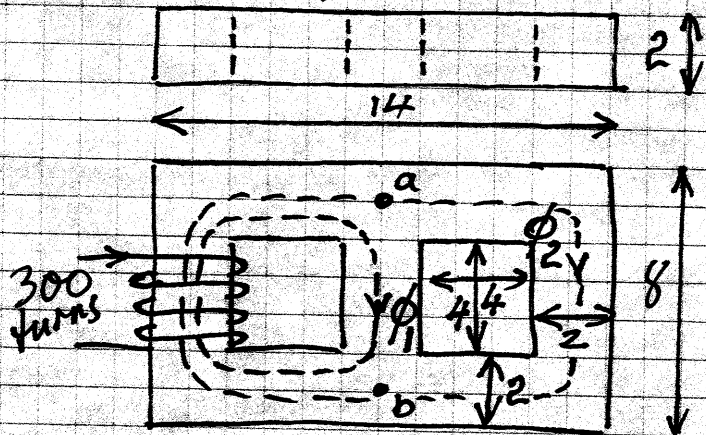
Note: A bit too high ($Ni = 600 \text{ A.t}$ specified)

Try $\frac{600}{618} \times 0.6 \text{ T}$ for new B.

Note: Problem is the non-linearity in Fig 20.16
 $\rightarrow \mu_{\text{core}}$ varies.

Example 7

Need $\phi_1 = 3.6 \times 10^{-4}$ Wb in center leg
Sheet steel core Find i



Dimensions in cm

$$\textcircled{1} \text{ Flux density in center leg} = B_1 = \frac{\phi_1}{A_1} = \frac{3.6 \times 10^{-4}}{0.02 \times 0.02} = 0.9 \text{ T}$$

$$\text{Fig 20.16} \rightarrow \text{For } B_1 = 0.9 \text{ T } H_1 = 150 \text{ A.t/m}$$

$$\text{so } \mathcal{F}_{ab} = H_1 l_1 = 150 \times 0.06 = 9 \text{ A.t.}$$

$$\textcircled{2} \text{ Similarly } H_2 = \mathcal{F}_{ab} / l_2 = \frac{9}{(6+6+6) \times 10^{-2}} = 50 \text{ A.t/m}$$

$$\text{From Fig 20.16 for } H_2 = 50 \text{ A.t/m } B_2 = 0.35 \text{ T so } \phi_2 = B_2 A_2$$

$$= 0.35 \times 4 \times 10^{-4} = 1.4 \times 10^{-4} \text{ Wb}$$

$$\textcircled{3} \text{ Left of } ab, \text{ Total flux } \phi = \phi_1 + \phi_2 = (3.6 + 1.4) \times 10^{-4} \text{ Wb} = 5 \times 10^{-4} \text{ Wb}$$

$$\& B = \frac{\phi}{A} = \frac{5 \times 10^{-4}}{4 \times 10^{-4}} = 1.25 \text{ T}$$

$$\text{From Fig 20.16 for } B = 1.25 \text{ T, } H = 500 \text{ A.t/m}$$

$$\& \mathcal{F} = H \cdot l = 500 \times 0.18 = 90 \text{ A.t.}$$

$$\uparrow 3 \times 0.06 \text{ m}$$

$$\therefore i = \frac{\mathcal{F} + \mathcal{F}_{ab}}{N} = \frac{90 + 9}{300} = 0.33 \text{ A}$$