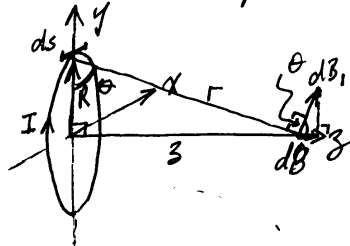
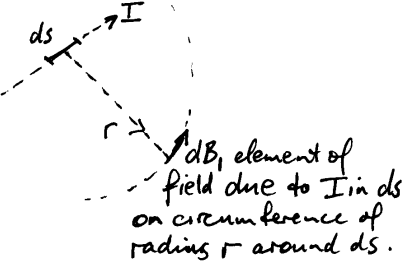


ECE 241 ASSIGNMENT #7

20.5 Circular coil, radius R , current I in x - y plane, center $(0,0)$
 Derive an expression for flux density \vec{B} as a function of z .



Detail of figure



Circular symmetry: only the axial component of $d\vec{B}_1$ is important i.e. $d\vec{B}$

$$dB = dB_1 \cos \theta \text{ due to } ds$$

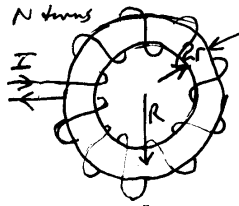
$$= \frac{\mu I ds}{4\pi r^2} \cos \theta = \frac{\mu I R}{4\pi r^3} ds$$

$$\therefore B = \frac{\mu I R}{4\pi r^3} \int ds$$

$$= \frac{\mu I R}{4\pi r^3} \cdot 2\pi R = \frac{\mu I R^2}{r^3}$$

$$= \frac{\mu I R^2}{(R^2 + z^2)^{3/2}}$$

20.12 Toroidal memory element (0/1 depends on magnetization direction)



Ferrite $\rightarrow \mu_f = 1100$ $R = 1 \text{ cm}$ $r = 0.1 \text{ cm}$

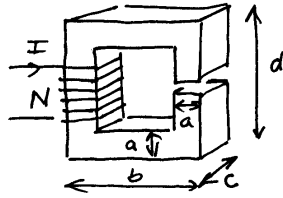
Find mmt for flux density 1.5 mT

$$F_{\text{mmt}} = \frac{1}{\mu} \frac{l}{A} \phi = \frac{1}{\mu} \frac{l}{A} BA = \frac{Bl}{\mu}$$

$$\therefore F = NI = \frac{B (2\pi R)}{\mu_r \mu_0} = \frac{1.5 \times 10^{-3} \times 2\pi \times 0.1 \times 10^{-2}}{1100 \times 4\pi \times 10^{-7}}$$

$$= 0.0068 = 6.8 \times 10^{-3} \text{ A.t}$$

20.21



Armco iron core $N=200$
 $a=5\text{cm}$ $b=d=20\text{cm}$ $c=10\text{mm}$

Find I for $\phi = 6.5\text{mWb}$, for

- (a) 5mm air gap
 (b) No air gap

$$(a) \quad B = \phi/A = \frac{6.5 \times 10^{-3}}{(5 \times 10^{-2})(10 \times 10^{-2})} = 1.3\text{T} \quad \text{assuming uniform area}$$

$$\text{For air gap: } \mathcal{F}_{\text{gap}} = H_{\text{gap}} l_{\text{gap}} = \left(\frac{B}{\mu_0} \right) l_{\text{gap}} = \frac{1.3}{4\pi \times 10^{-7}} 5 \times 10^{-3}$$

$$= 5.17 \times 10^3 \text{ A}\cdot\text{t}$$

is neglecting fringing.
 $A = c \cdot a$

$$\text{For the iron: Average } l_i = 2(d-a) + 2(b-a) - 5\text{mm}$$

$$= 2(20-5) + 2(20-5) - 0.5 \text{ cm}$$

$$= 0.55\text{m}$$

From Fig 20.16 For Armco iron:

$$B_i = 1.3\text{T} \rightarrow H_i \approx 250 \text{ A}\cdot\text{t/m}$$

$$\therefore \mathcal{F}_i = H_i l_i = 250 \times 0.55 = 137.5 \text{ A}\cdot\text{t}$$

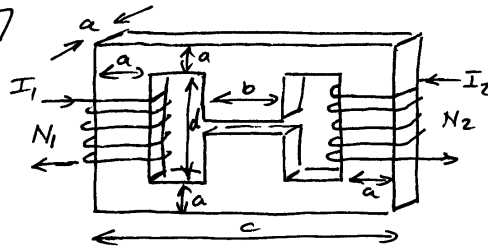
$$\therefore I = (\mathcal{F}_{\text{gap}} + \mathcal{F}_i) / N = \frac{5170 + 137.5}{200} = \frac{5307.5}{200} = 26.54\text{A}$$

$$(b) \text{ No air gap } \mathcal{F} = \mathcal{F}_i = H_i l_i = 250 \times 0.6 = 150 \text{ A}\cdot\text{t}$$

$$\therefore I = \mathcal{F} / N = 150 / 200 = 0.75\text{A}$$

Compare 0.75A for no gap with 26.54A with gap.

20.27



Silicon sheet steel
with 5mm air gap

$$a = 20\text{cm} \quad b = 40\text{cm}$$

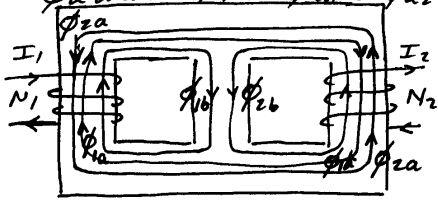
$$c = 120\text{cm} \quad d = 60\text{cm}$$

$$N_1 = N_2 = 500 \text{ turns}$$

Find $I_1 = I_2$ for 100 mWb in gap.

[Note: Hint about symmetry!]

Compare Example 7: separate Φ_a due to I_1 into Φ_{a1} & Φ_{a2}



Note directions of magnetic field due to I_1 and I_2 above.
RH rule: both produce B "upwards" in coil.

Φ_{a1}, Φ_{a2} cancel in both outer legs, leaving only $\Phi_{b1} + \Phi_{b2}$ in center leg.

Assume $F_{\text{airgap}} \Rightarrow F_{\text{iron}}$

$$\therefore 2NI = N_1 I_1 + N_2 I_2$$

$$= H_{\text{gap}} l_{\text{gap}}$$

$$= \frac{B_{\text{gap}}}{\mu_0} l_{\text{gap}} = \frac{\Phi_{\text{gap}}}{A_{\text{gap}} \mu_0} l_{\text{gap}}$$

$$A_{\text{gap}} \approx ab = (20 \times 10^{-2} \times 40 \times 10^{-2})$$

$$\therefore I_1 = I_2 = \frac{1}{2N} \frac{\Phi}{A_{\text{gap}}} \frac{l_{\text{gap}}}{\mu_0} = 10^{-3} \frac{100 \times 10^{-3}}{8 \times 10^{-2}} \frac{0.5 \times 10^{-2}}{4\pi \times 10^{-7}} = 4.97 \text{ A}$$

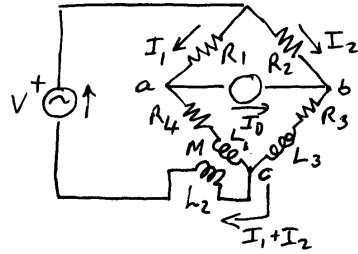
(neglecting fringing.)

$$\text{Including fringing } A_{\text{gap}} \rightarrow 20.5 \times 40.5 \times 10^{-4} = 8.3025 \times 10^{-2}$$

$$I_1 = I_2 \rightarrow 4.79 \text{ A}$$

For each winding, could consider the extra mmt required by the core flux but complicated by effective μ_{iron} (Fig 20.16) and zero net flux areas.

20.32



Find M (mutual inductance between coils 1 & 2) when $I_D = 0$

$$I_D = 0 \therefore V_a = V_b$$

$$\therefore I_1 R_1 = I_2 R_2$$

$$\therefore I_2 = \frac{R_1}{R_2} I_1$$

$$\& V_{ac} = V_{bc} \therefore I_1 (R_4 + j\omega L_1) + j\omega M (I_1 + I_2) = I_2 (R_3 + j\omega L_3)$$

$$I_1 (R_4 + j\omega L_1) + j\omega M I_1 \left(1 + \frac{R_1}{R_2}\right) = \frac{R_1}{R_2} I_1 (R_3 + j\omega L_3)$$

$$R_4 + j\omega \left(L_1 + M + \frac{R_1}{R_2} M\right) = \frac{R_1 R_3}{R_2} + j\omega L_3 \frac{R_1}{R_2}$$

Equating real and imaginary parts : $R_4 = \frac{R_1 R_3}{R_2}$

and $L_1 + M + \frac{R_1}{R_2} M = L_3 \frac{R_1}{R_2}$

gives $M = \frac{L_3 \frac{R_1}{R_2} - L_1}{1 + R_1/R_2} = \frac{R_1 L_3 - R_2 L_1}{R_1 + R_2}$