# Heat Transfer from a Single, Heated Block

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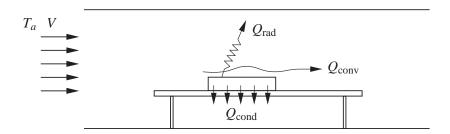
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# **Overview**

- Schematic of Basic Experiment
- Measuring the Heat Transfer Coefficient
- Heater Circuit
- Experiment Planning
- Uncertainty analysis
- Relationship to Practical Thermal Management Problems

# Measurement of Heat Transfer Coefficient (1)



Calculate the heat transfer coefficient from measured quantities

$$h = \frac{Q_{\text{conv}}}{A_s(\bar{T}_s - T_a)} \tag{1}$$

where

 $T_s =$  average surface temperature of the block

 $T_a =$  temperature of air approaching the block

 $A_s =$  surface area of block that is participating in the

convection

 $Q_{
m conv} = -$  convective heat loss from the block

# Measurement of Heat Transfer Coefficient (2)

Not all of the electrical power input is lost directly by convection.

An energy balance on the block gives

$$Q_{\text{conv}} = \dot{E}_{\text{in}} - Q_{\text{cond}} - Q_{\text{rad}}$$
 (2)

 $Q_{\mathrm{conv}} =$  convective heat loss

 $\dot{E}_{
m in} = -$  electrical power input

 $Q_{
m cond} = \;\;$  conduction heat transfer from block to

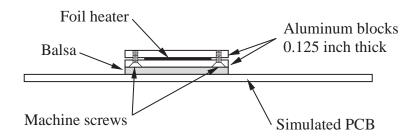
board

 $Q_{
m rad} =$  radiation heat transfer to surroundings

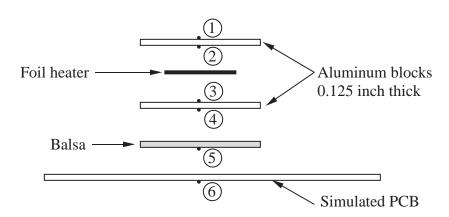
Equation (2) is a centering correction.

# **Device Mock-up**

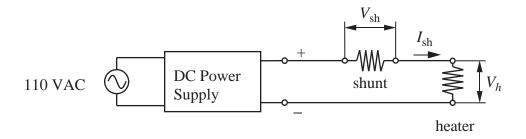
## Heater assembly:



Exploded view with potential temperature measurement locations:



# Measuring Power Input (1)



The power dissipated by the electric resistance heater is

$$\dot{E}_{\rm in} = V_h I_h \tag{3}$$

where  $V_h$  is the voltage across the heater, and  $I_h$  is the current through the heater. The shunt resistor is used to measure  $I_h$ . From a measurement of  $V_{\rm sh}$  we compute

$$I_h = I_{\rm sh} = \frac{V_{\rm sh}}{R_{\rm sh}} \qquad \Longrightarrow \quad \dot{E}_{\rm in} = \frac{V_h V_{\rm sh}}{R_{\rm sh}}$$
 (4)

# Measuring Power Input (2)

Measuring power with a shunt resistor is much more accurate than measuring just the voltage across the heater and computing  $\dot{E}_{\rm in}=V_h^2/R_h$  because  $R_h$  varies with temperature.

The shunt resistor has a very low and stable resistance  $(R_{\rm sh} \sim 0.005\,\Omega)$ . Since  $R_{\rm sh}$  is very small, the shunt resistor dissipates very little power. Thus its temperature will be stable and its resistance will not change during the experiment.

# Measuring Power Input (3)

#### **Sample Power Calculation:**

Assume that  $R_{\rm sh}=0.005\,\Omega$  and that  $V_{\rm sh}=2.8\times 10^{-3}$  V and  $V_h=8.5$  V were measured. Then

$$\dot{E}_{\rm in} = \frac{(8.5)(2.8 \times 10^{-3})}{0.005} = 4.76 \,\rm W$$

and

$$E_{\text{shunt}} = \frac{V_{\text{shunt}}^2}{R_{\text{sh}}}$$

$$= \frac{(2.8 \times 10^{-3})^2}{0.005} = 1.57 \times 10^{-3} \,\text{W}$$

## **Experiment Planning**

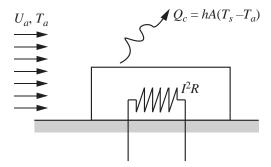
1. Decide which type of sensors, and how many of each type are needed to measure all quantities used to compute h from

$$h = \frac{Q_{\text{conv}}}{A(\bar{T}_s - T_a)}$$

- 2. Develop a wiring diagram for your experiment.
- 3. Fabricate thermocouples and attach them to your apparatus.
- 4. Mount your apparatus to a bottom hatch for the wind tunnel.
- 5. Route the sensor leads to a terminal strip. Label all wires and document the labeling scheme in your notebook and your report.

# Model of Start-up Transient (1)

How long will you have to wait for steady state?



Use a simplified model to estimate the time it takes the block to reach its steady state temperature.

## **Assumptions:**

- Block has uniform temperature
- All heat is lost by convection

# Model of Start-up Transient (2)

A transient energy balance on the block gives

$$mc\frac{dT}{dt} = \dot{E}_{\rm in} - hA(T - T_a) \tag{5}$$

where  $\dot{E}_{\rm in}$  is the electrical power input, h is the heat transfer coefficient. Use a shifted temperature  $\theta$ , and the response time au

$$\theta = T - T_a \qquad \tau = \frac{mc}{hA} \tag{6}$$

to transform Equation (5) to dimensionless form

$$\frac{d\theta}{dt} = \frac{\dot{E}_{\rm in}}{mc} - \frac{\theta}{\tau} \tag{7}$$

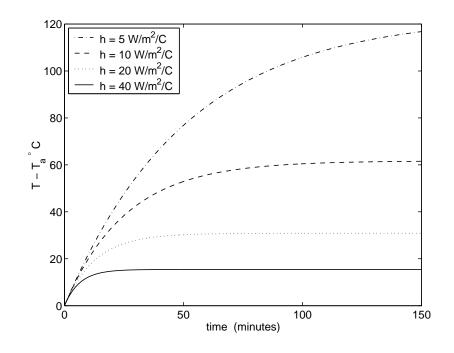
# Model of Start-up Transient (3)

With the initial condition

$$\theta(t=0) = \theta_i = T_i - T_a$$

the solution to Equation (7) is

$$\theta = \frac{\dot{E}_{\rm in}}{hA} + \left(\theta_i - \frac{\dot{E}_{\rm in}}{hA}\right) e^{-t/\tau}$$



# Model of Start-up Transient (4)

Define  $T_{
m ss}$  as the steady state temperature

$$T_{
m ss} = T_a + rac{\dot{E}_{
m in}}{hA}$$

and  $t_p$  as the time for block to reach p percent of its final temperature difference

$$\frac{T - T_a}{T_{\rm ss} - T_a} = \frac{p}{100}$$

With our model we compute

| h                           | au    | $T_{ m ss}$            | $t_{50}$ | $t_{90}$ | $t_{99}$ |
|-----------------------------|-------|------------------------|----------|----------|----------|
| $(\mathrm{W/m^2/^\circ C})$ | (min) | $(^{\circ}\mathrm{C})$ | (min)    | (min)    | (min)    |
| 5                           | 51    | 143                    | 36       | 118      | 236      |
| 10                          | 26    | 82                     | 18       | 59       | 118      |
| 20                          | 13    | 51                     | 9        | 30       | 59       |
| 40                          | 6     | 35                     | 4        | 15       | 30       |

# **Uncertainty Analysis (1)**

Suppose that your data reduction equation had the form

$$h = f(V_h, V_{\rm sh}, R_{\rm sh}, A_s, T_a, T_w, T_{\rm bt}, T_{\rm bb}, k_b, \varepsilon)$$
(8)

 $V_h =$  voltage across the heater

 $V_{
m sh} = ext{voltage across the shunt resistor}$ 

 $R_{
m sh} = -$  resistance of shunt resistor

 $A_s =$  surface area of the block

 $T_a =$  temperature of oncoming air

 $T_w =$  temperature of duct walls

 $T_{
m bt} = -$  temperature on the top surface of the board

 $T_{
m bb} = ext{temperature on the bottom surface of the board}$ 

 $k_b =$  thermal conductivity of the board

 $\varepsilon =$  emissivity of the heated block

Data analysis involves creating a routine to compute h, and perturbation of all inputs to estimate  $u_h$ .

# **Uncertainty Analysis (2)**

Given the data reduction formula in Equation (8)

$$u_{h_{V_h}} = f(V_h + u_{V_h}, V_{sh}, R_{sh}, A_s, T_a, T_w, T_{bt}, T_{bb}, k_b, \varepsilon) - h$$

$$u_{h_{V_{sh}}} = f(V_h, V_{sh} + u_{V_{sh}}, R_{sh}, A_s, T_a, T_w, T_{bt}, T_{bb}, k_b, \varepsilon) - h$$

$$\vdots$$

$$u_h = \sqrt{(u_{h_{V_h}})^2 + (u_{h_{V_{sh}}})^2 + \dots}$$

where

 $u_{V_{
m h}}$  the *total* uncertainty in the heater voltage  $u_{V_{
m sh}}$  the *total* uncertainty in the voltage across the shunt resistor

 $u_{V_h}$ ,  $u_{V_{
m sh}}$ , etc. depend on random error, instrument error, and calibration error.

### Shakedown

An end-to-end calibration is also called first order replication

- Used to verify equipment
- Make measurements of known quantities

  - ▶ Perform benchmark experiments: Can you repeat experiments and obtain the same results published by others?
- One outcome is an estimate of random component of fixed error

  - ▶ Wait for system to come into steady state
  - ▷ Over time period of typical data collection, take 30 (or more) samples from each sensor

  - $\triangleright~u_{x_{
    m random}}=2\sigma$  for 20:1 odds (95 % confidence)

## Relationship to Practical Problems

- Heaters as Prototype Devices
- Develop experience with multimode heat transfer
- Gain familiarity with complexity of measurements
- Gain experience building a thermal mock-up

## References

[1] R. J. Moffat. Uncertainty analysis. In K. Azar, editor, *Thermal Measurements in Electronic Cooling*, pages 45–80. CRC Press, Boca Raton, FL, 1997.