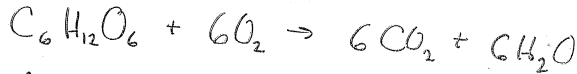


THEORETICAL OXYGEN DEMAND

(BASED ON SIMPLE STOICHIOMETRY)

GLUCOSE IN WATER



↑ FW = 180 ↑ FW = 32

SUPPOSE A DILUTE WASTEWATER

FROM A FOOD PLANT:

GLUCOSE = 1 mg/L

$$\frac{1 \frac{mg}{L}}{180 \frac{mg}{mol}} = 0.0055 \text{ mM}$$

↓ REACTS w/ 6 O₂'s

$$0.0055 \text{ mM} \times 6 = 0.033 \text{ mM O}_2 \text{ CONSUMED}$$

$$0.033 \times 32 \frac{mg}{mmol} = 1.1 \text{ mg-O}_2/L$$

$$\text{BOD} = 1.1 \text{ mg/L}$$

BOD

① PURE SAMPLE IN BOTTLE

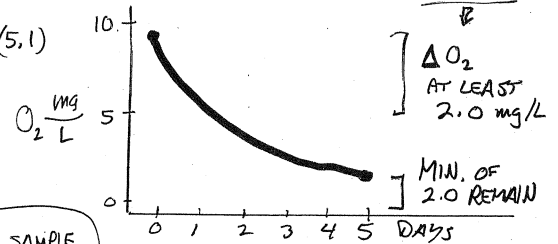
$$BOD_5 = DO_i - DO_5$$

② Dilution usually needed

$$P = \frac{\text{Volume of Wastewater}}{\text{Vol. of WW} + \text{Vol. Diln Water}}$$

$$BOD_5 = \frac{DO_i - DO_5}{P}$$

EXAMPLE (5.1)



10 mL SAMPLE
300 mL BOTTLE

$$\text{MIN. BOD}_5 = \frac{\Delta DO}{P} = \frac{2.0 \text{ mg/L}}{10/300} = 60 \text{ mg/L}$$

$$\text{MAX BOD} = \frac{9.0 - 2.0}{10/300} = 210 \text{ mg/L}$$

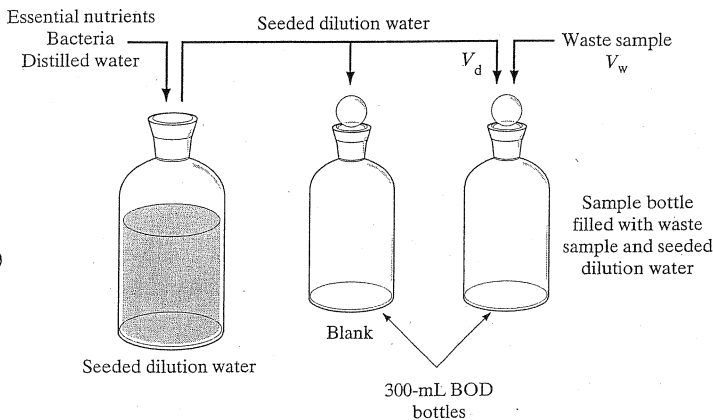


FIGURE 5.9 Laboratory test for BOD using seeded dilution water.

SEEDED BOD TEST

"w" = waste "d" = dil'n water "m" = mixture

$$BOD_m V_m = BOD_w V_w + BOD_d V_d$$

$$BOD_w = BOD_m \left(\frac{V_m}{V_w} \right) - BOD_d \left(\frac{V_d}{V_w} \right) \left(\frac{V_m}{V_w} \right)$$

$$BOD_w = \frac{BOD_m}{V_w/V_m} - BOD_d \frac{V_d/V_m}{V_w/V_m} \leftarrow 1-P$$

$$\uparrow P = V_w/V_m$$

$$BOD_w = \frac{BOD_m - BOD_d(1-P)}{P}$$

$$\text{OR } BOD_w = \frac{(DO_i - DO_f) - (B_i - B_f)(1-P)}{P}$$

EXAMPLE

$$15 \text{ mL SAMPLE IN } 300 \text{ mL BOTTLE } \left\{ P = \frac{15}{300} = 0.05 \right.$$

$$\Delta DO_B = 1.0 \text{ mg/L} \quad \Delta DO_{\text{SAMPLE}} = 7.2 \text{ mg/L}$$

$$BOD_5 = \frac{7.2 - 1.0(1-0.05)}{0.05} = 125 \text{ mg/L}$$

BOD MODEL: 1st ORDER DECAY

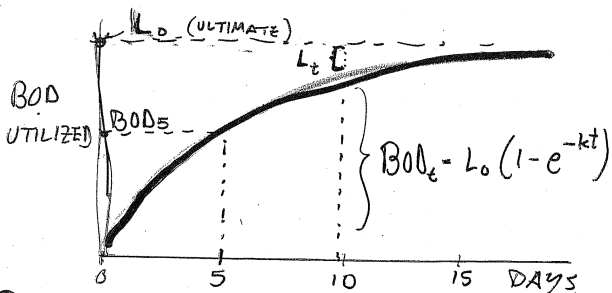
L_t = oxygen demand remaining @ t
 L_0 = ultimate (100%) oxygen demand (Carbonaceous)

$$L_t = L_0 e^{-kt}$$

$$L_0 = \text{BOD}_t + L_t$$

↑ ULTIMATE DEMAND
 ↑ DEMAND "USED UP" By t
 ↑ DEMAND REMAINING AT t

$$\text{BOD}_t = L_0 - L_0 e^{-kt} = L_0 (1 - e^{-kt})$$



Also: $\text{BOD}_t = L_0 (1 - 10^{-kt})$ $k = K \ln 10 = 2.303K$

TEMP. DEPENDENCE OF BOD

At 20°C

	k (d ⁻¹)
RAW SEWAGE	0.35 - 0.70
TREATED SEWAGE	0.12 - 0.23
POLL. RIVER	0.12 - 0.23

$$k_T = k_{20} \theta^{(T-20)}$$

$\theta = 1.047$ typical

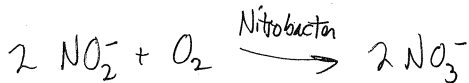
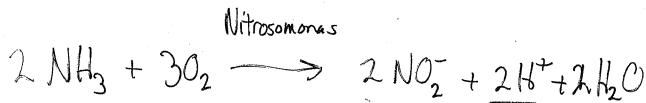
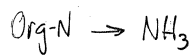
EX: At 20°C $\text{BOD}_0 = 300 \text{ mg/L}$
 $\text{BOD}_5 = 200 \text{ mg/L}$
 $k = 0.22 \text{ d}^{-1}$

$\text{BOD}_5 @ 25^\circ ?$

$$k_{25} = k_{20} \theta^{T-20} = 0.22 (1.047)^{(25-20)} = 0.277 \text{ d}^{-1}$$

$$\text{BOD}_5 = L_0 (1 - e^{-kt}) = 300 (1 - e^{-0.277 \times 5}) = 225 \text{ mg/L}$$

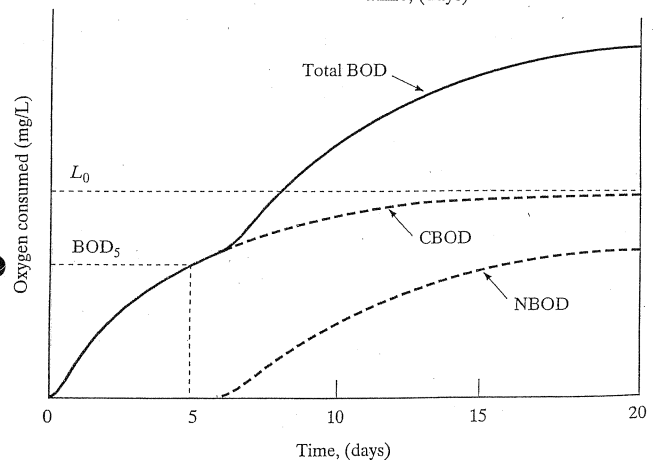
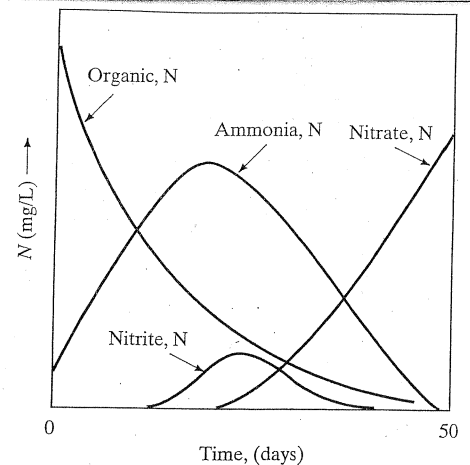
NITRIFICATION



"NBOD"

Usually we try to NOT measure this in standard BOD_5 (Hence 5-day limit)

BOD tends not to be a serious problem in many rivers unless is very high or river has very high loading.



E 5.13 Illustrating the carbonaceous and nitrogenous biochemical oxygen demand. Total BOD n of the two.